



Réunion ANR DIP-NAWDEX 2020

Diabatic processes in the Warm Conveyor Belt of the Stalactite Cyclone

Sensitivity to the two deep convection schemes in
ARPEGE

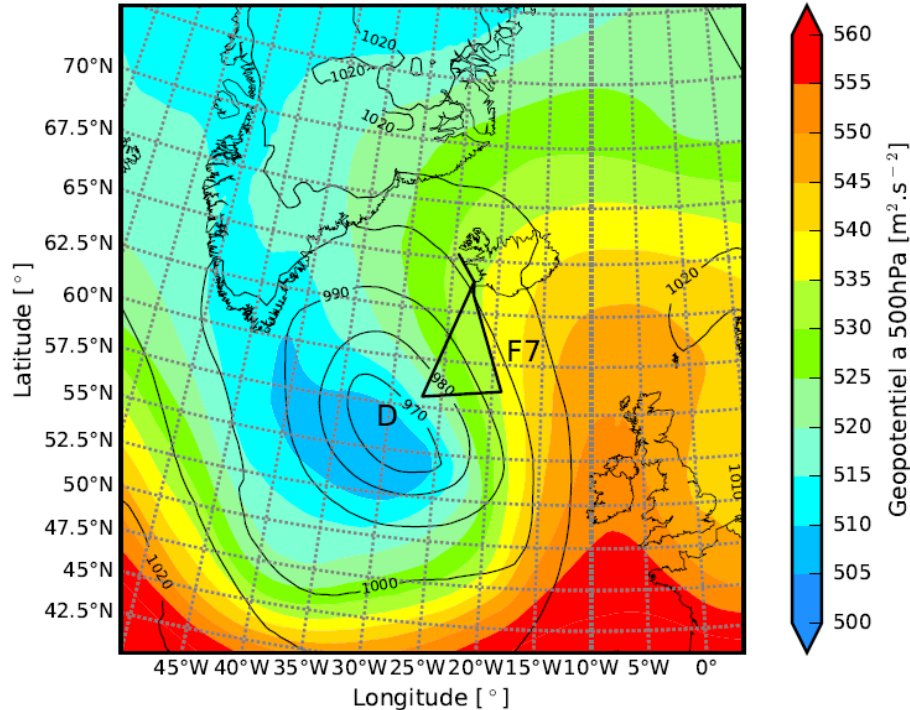
Meryl WIMMER

Centre National de Recherches Météorologiques
25/02/2020, Toulouse

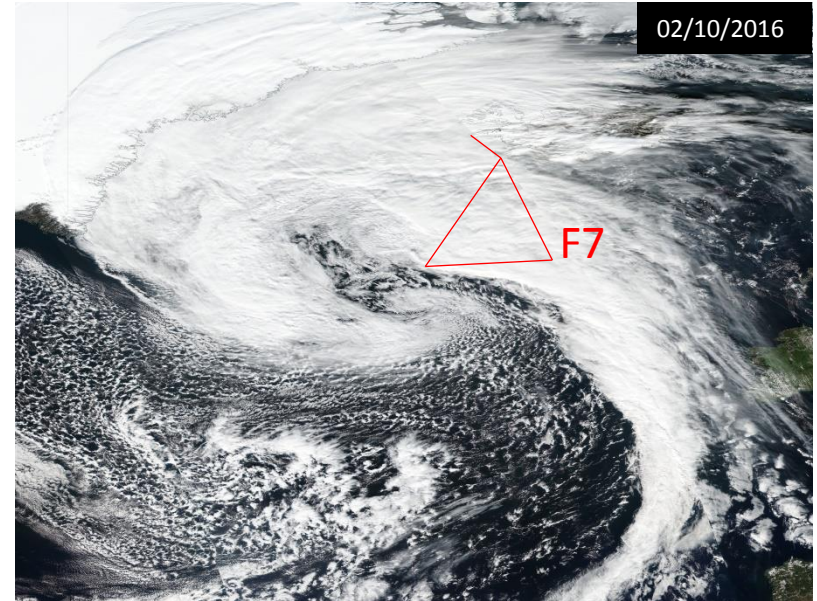
G. Rivière, P. Arbogast, J.-M. Piriou, J. Delanoë, Q. Cazenave, J. Pelon, C. Labadie

Stalactite Cyclone

Geopotential at 500 hPa and Mean Sea Level Pressure



ARPEGE Analysis, 02/10/2016 at 12h UTC



MODIS, Nasa Worldview Application

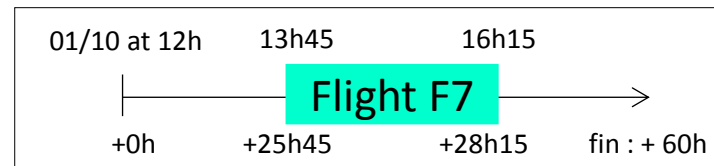
ARPEGE-EPS (cy41.op1)

NWP :

- Resolution : 10km on France, 20km on Islande (TL798 C2.4)
- Level : 90 from 14m to 50km (1hPa)
- Time step : 514,3s
- Initial Condition : ARPEGE analysis of the 01/10/2016 at 12h UTC

Outputs :

- Resolution : 0,5°
- Level : model grid
- Time step : 15min
- Heating and PV tendencies



Deep convection scheme in ARPEGE-EPS

Bougeault, 1985 (B85)

- Mass-Flux scheme
- Closure : moisture

Piriou et al, 2007 (PCMT)

- Mass-Flux scheme
- Closure : CAPE
- Microphysic and transport schemes
- Strong entrainment

Shallow convection : KFB (Bechtold et al. 2001) // PMMC (Pergaud et al. 2009)

Influence of these two deep convection schemes on the Stalactite Cyclone WCB

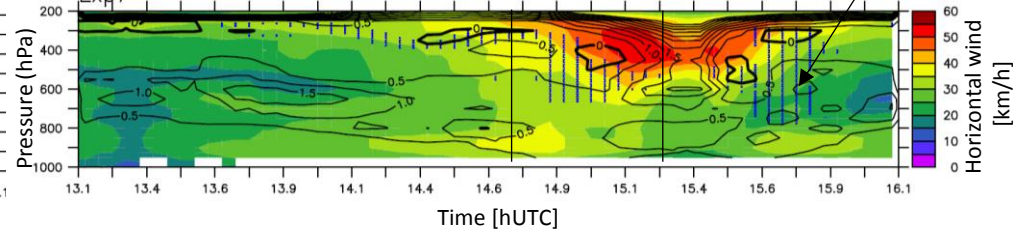
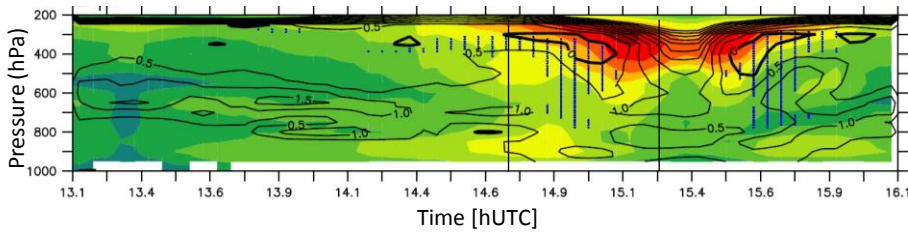
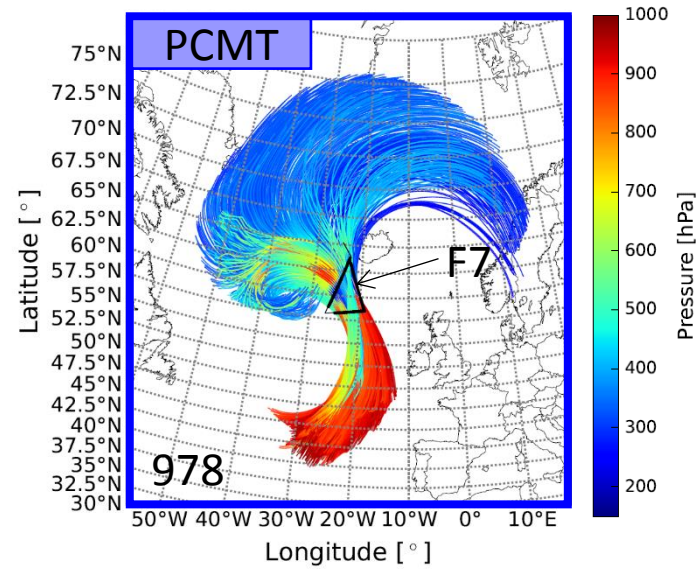
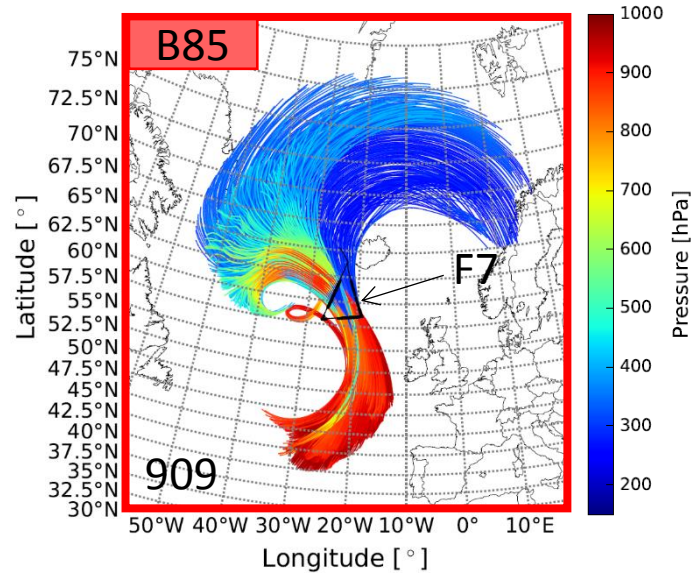
Research questions

- Along the flight track, in particular in the WCB region, what are the differences in PV and wind between the two convection schemes ?
- Which scheme is closer to the observations ?
- What are the difference between the two convection scheme in the upper level ridge building ?

Warm Conveyor Belt – Flight F7

Trajectories : -24h / +24h

WCB : -300hPa in 24h for every 24h in 48h of trajectory + $P_0 > 850\text{hPa}$

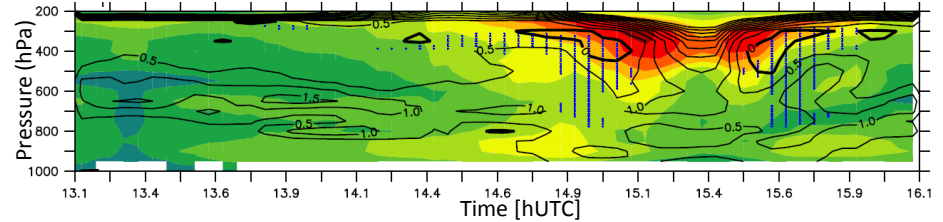
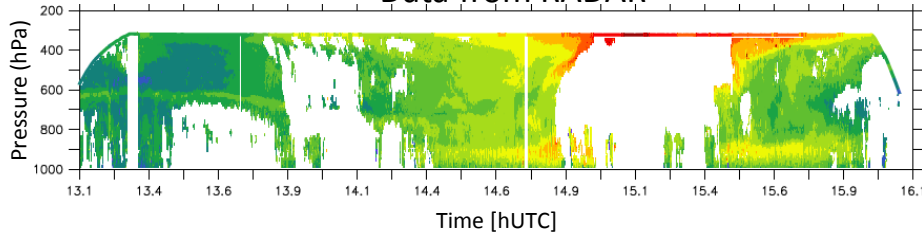


Wind Observations from RADAR / Model

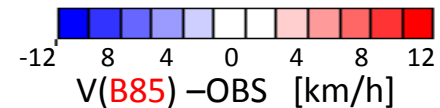
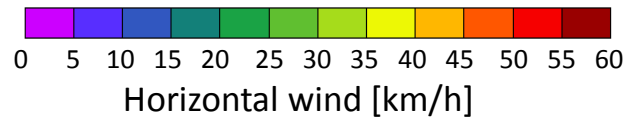
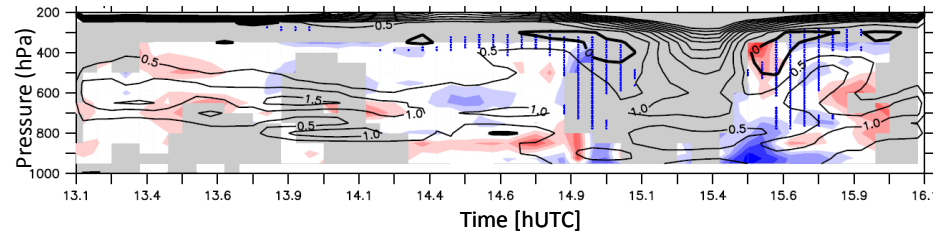
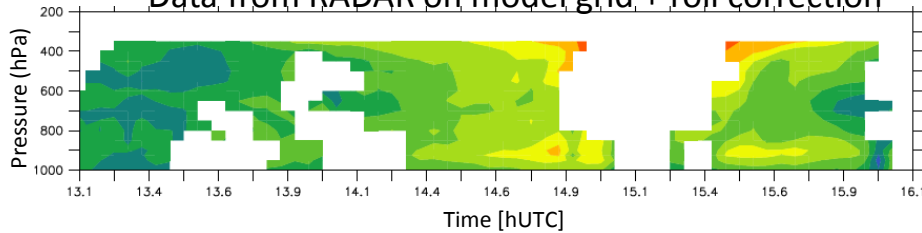
Observations

Model : **B85**

Data from RADAR



Data from RADAR on model grid + roll correction

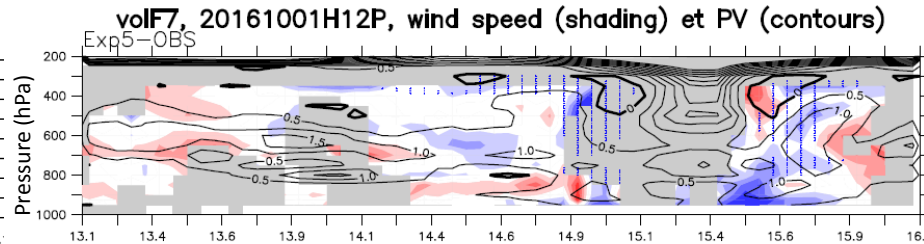
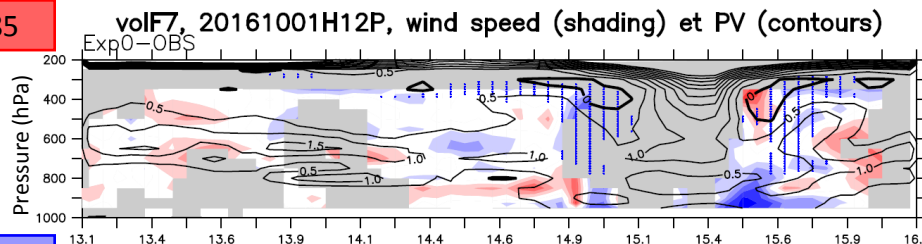


Link between PV and wind

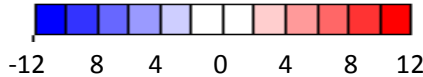
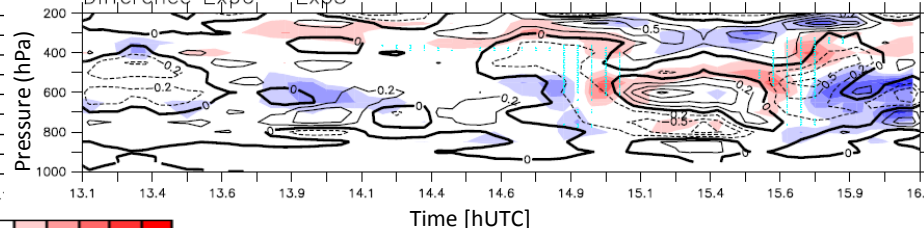
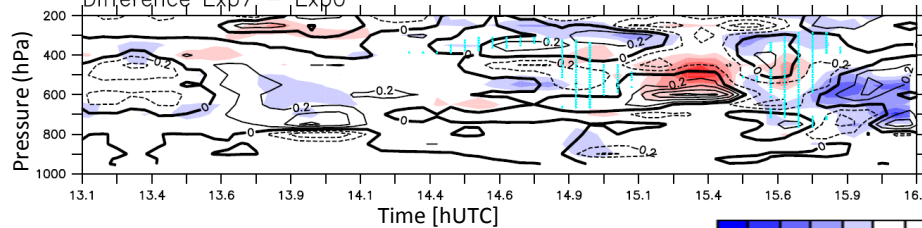
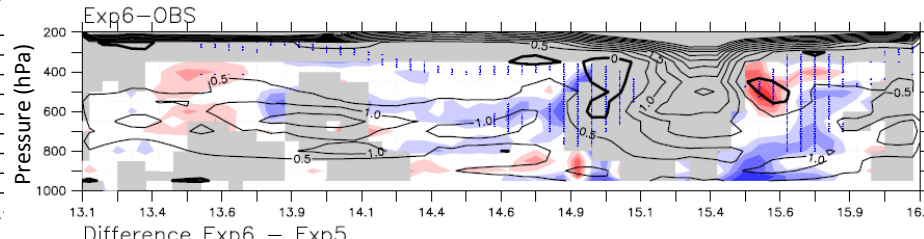
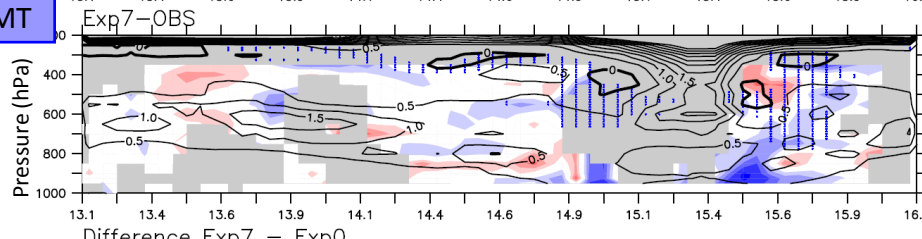
KFB

PMMC

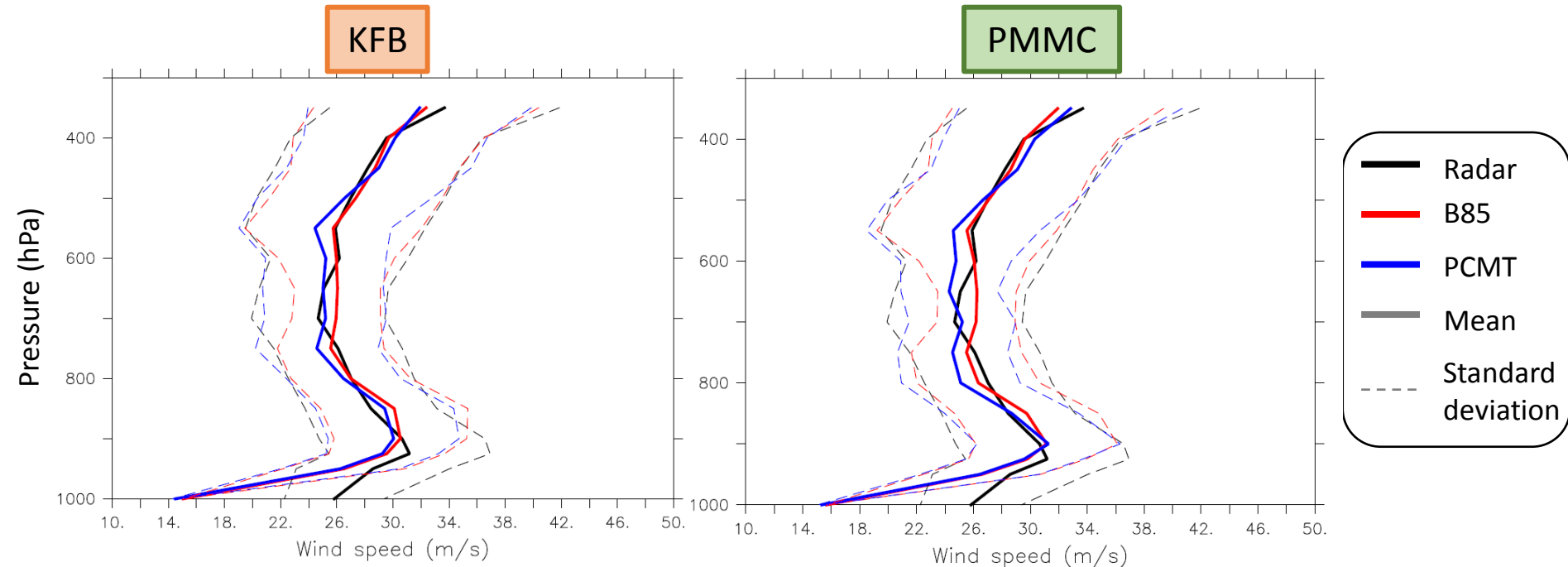
B85



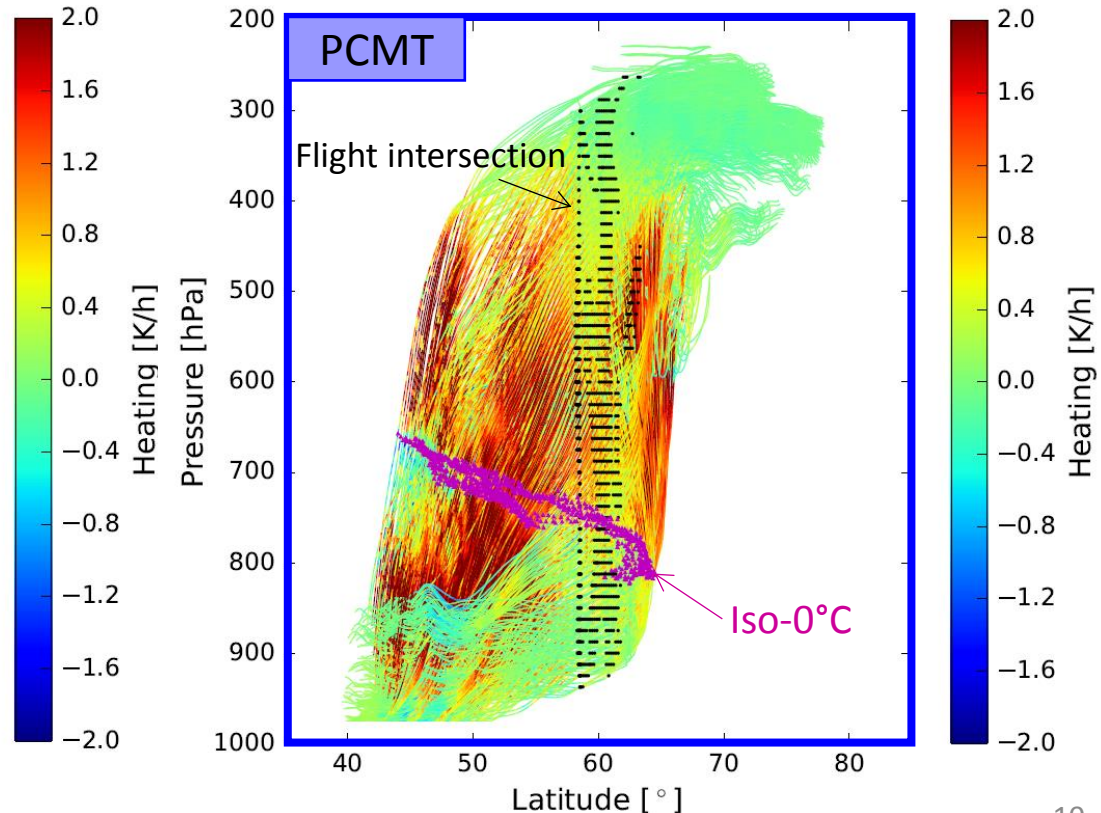
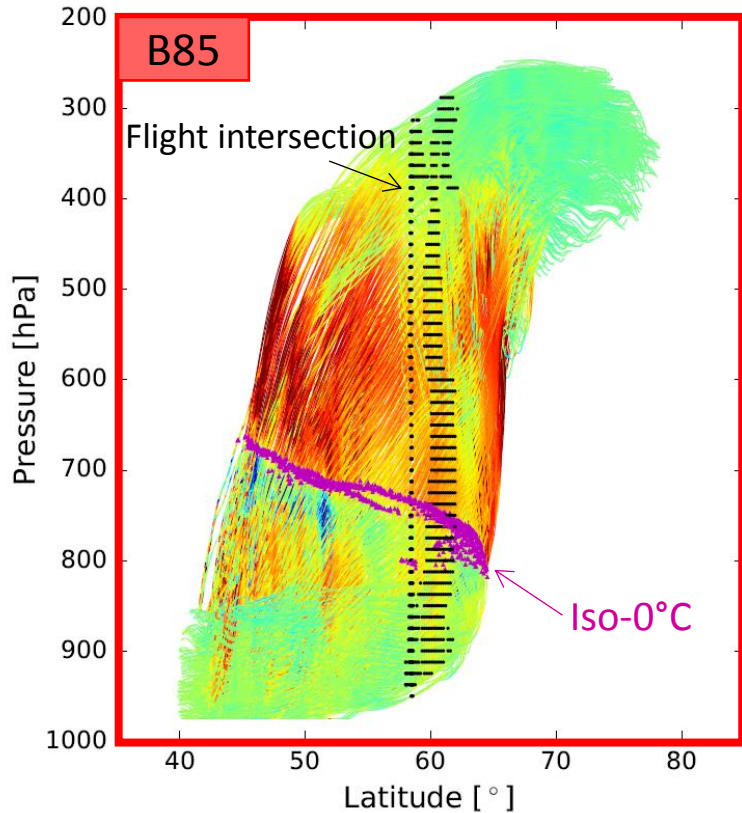
PCMT



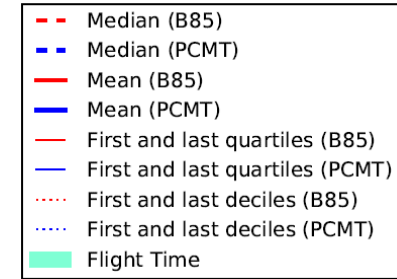
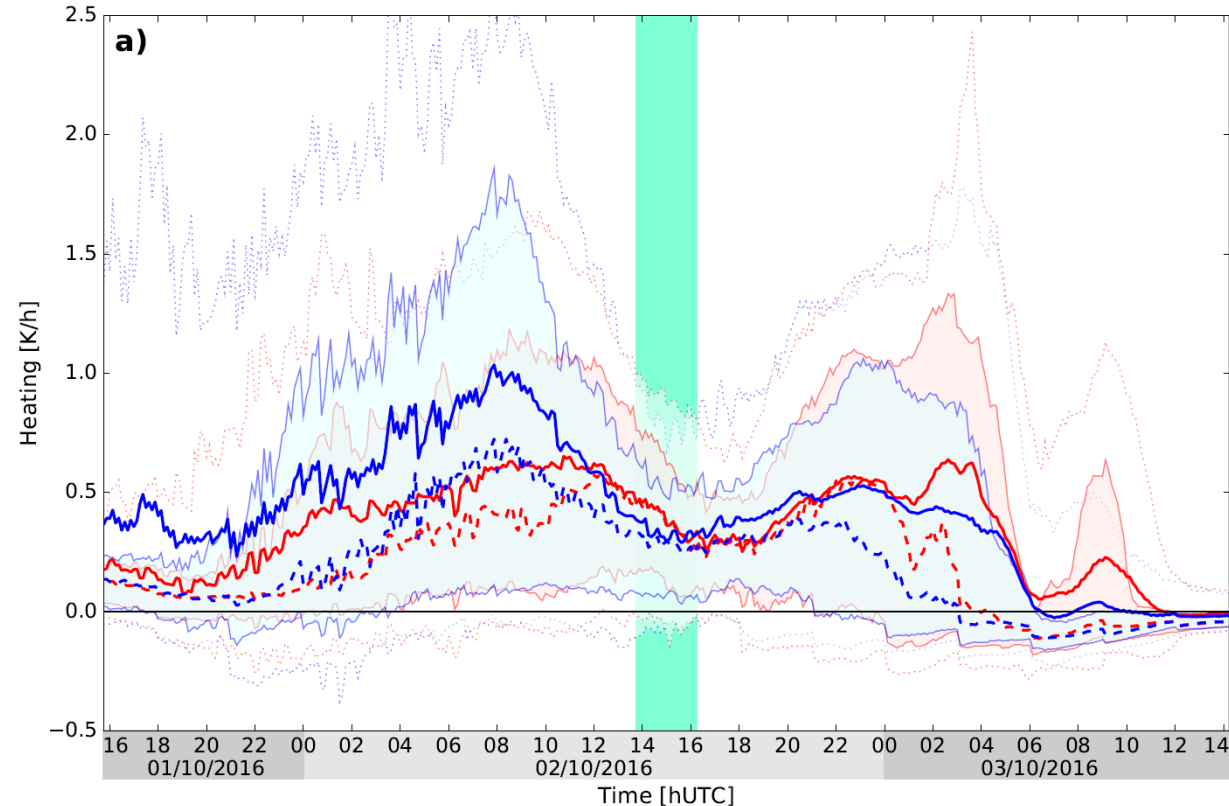
Wind profile where there is observation



Different heating in the liquid phase



Evolution in time of the heating

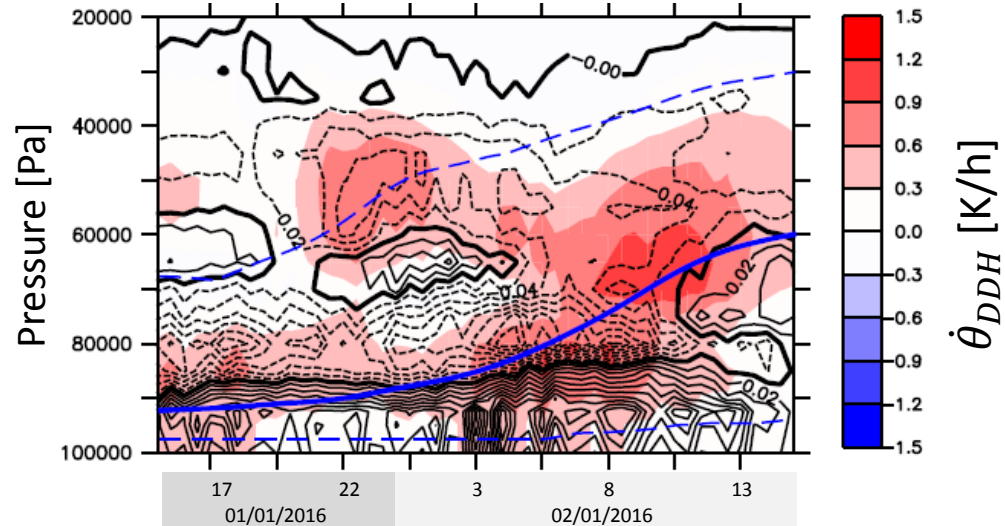
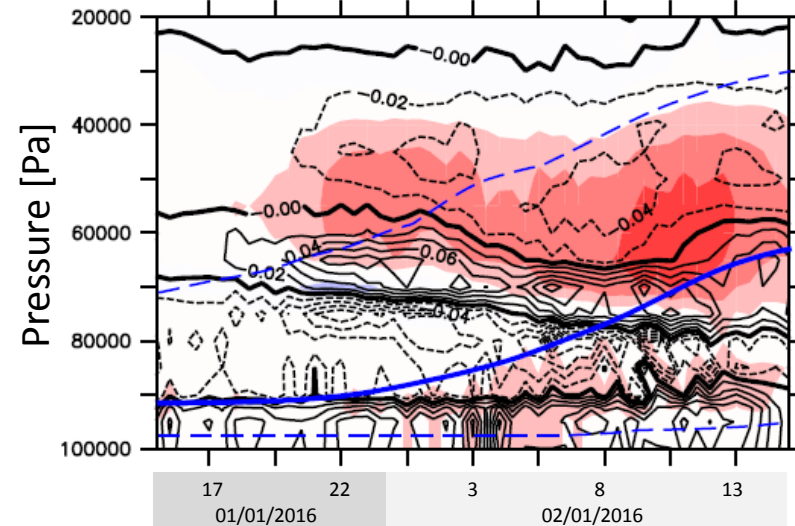


Sooner heating in PCMT
 Later heating in B85

Vertical profile of mean heating and $P\dot{V}$ along WCB trajectories

B85

PCMT



Trajectories below the heating

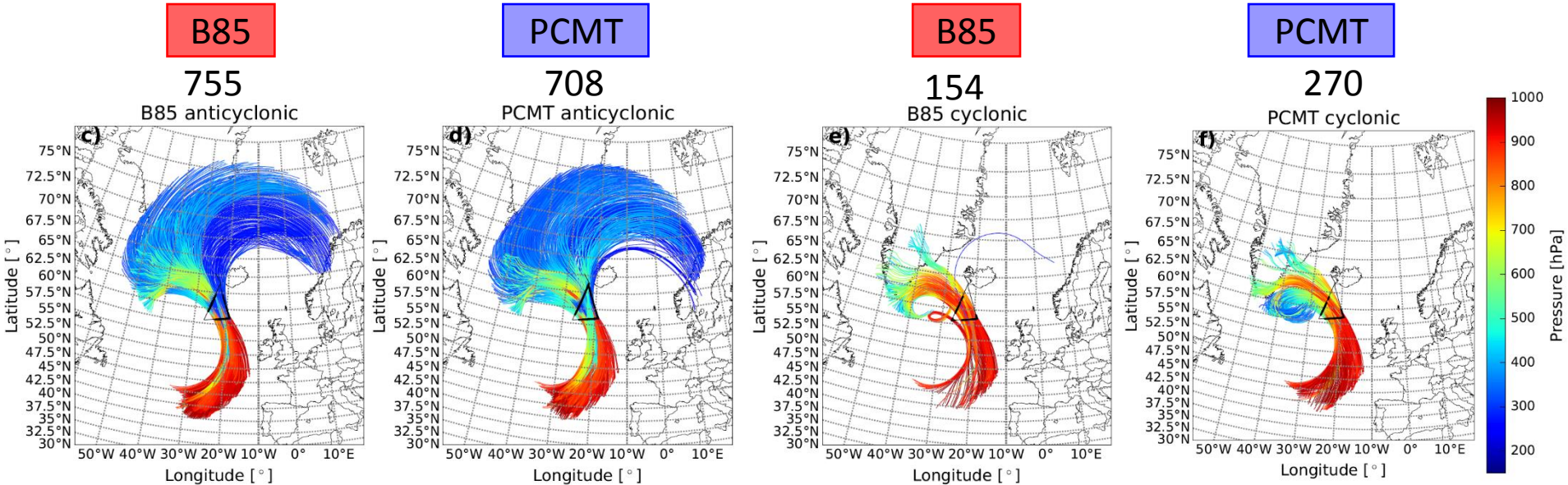
Lower Heating

-> many trajectories in the $PV < 0$ part

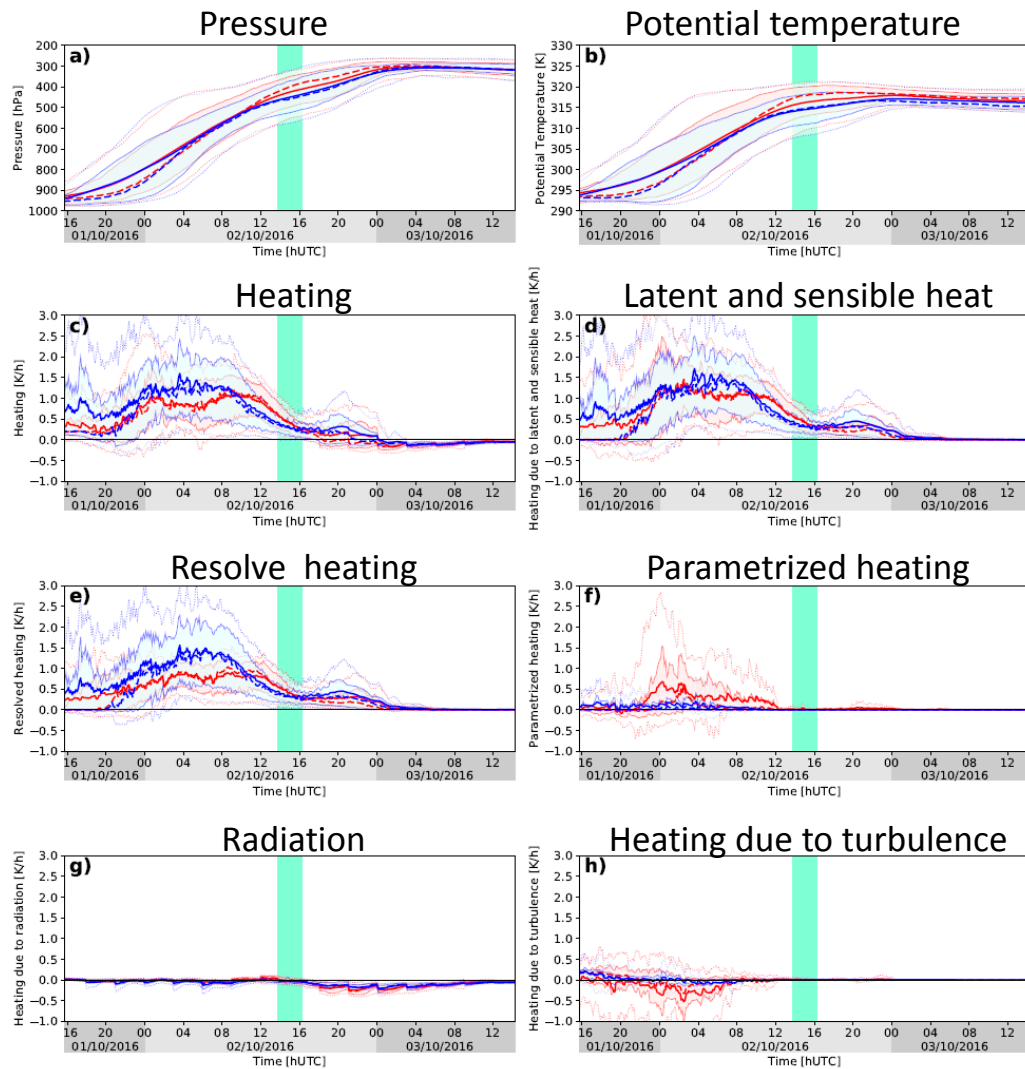
Separation anticyclonic/cyclonic trajectories

Mean direction during 3h -> to the left : cyclonic

-> to the right : anticyclonic



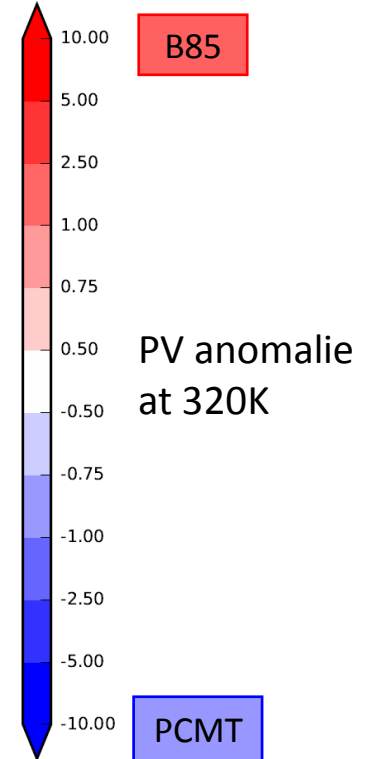
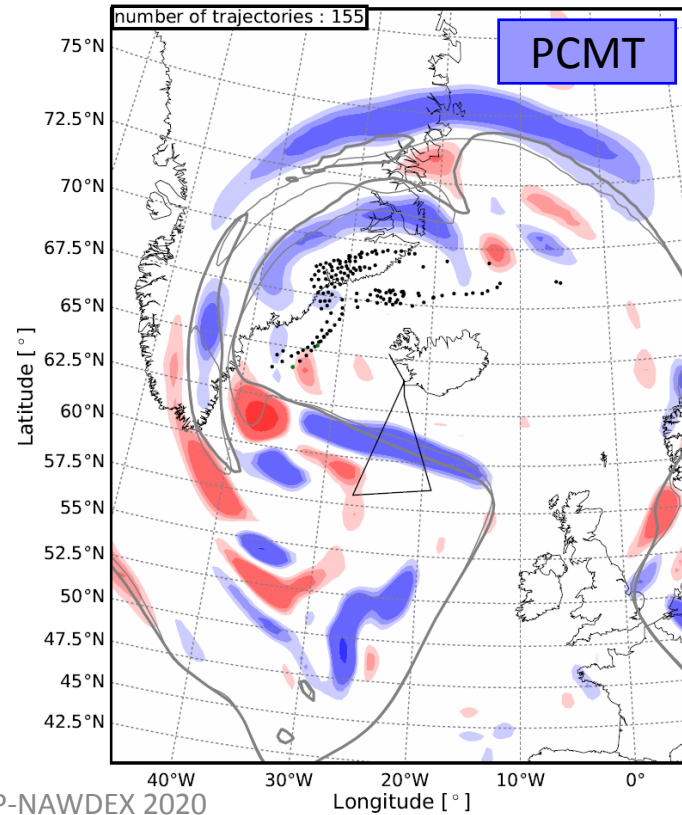
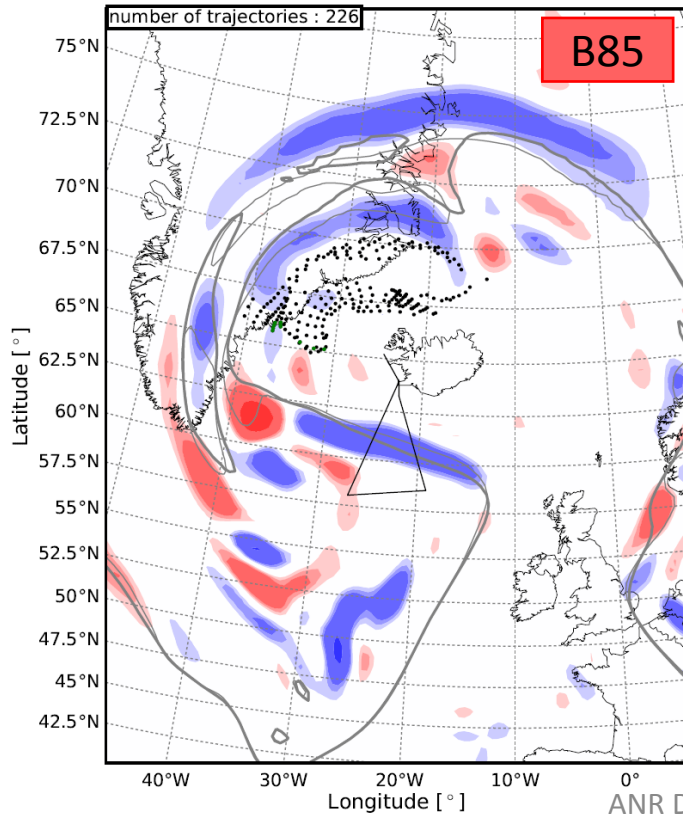
Heating budget for anticyclonic trajectories above 315K



Heating in ice phase from parametrization with B85

Ridge Building

Trajectories between 317-323K (+36h)



Differences between B85/PCMT

B85

- Upper Heating
- Ice phase heating (higher IWC)
- In the flight:
 - Trajectories are still below the heating
 - Still production of PV
- After the flight:
 - Heating due to ice phase
 - Higher and more trajectories which bring PV – in high altitude
 - Higher and stronger anticyclone at later stage

PCMT

- Earlier and lower Heating
- Liquid phase heating
- In the flight:
 - Trajectories inside the heating
 - More destruction of PV
- After the flight:
 - Less trajectories in upper levels
 - Weaker anticyclone at later stage

Perspectives

Short-term: (article)

- Improve heating and PV budget
- Create generic WCB trajectories (from warm sector)

Long-term:

- Study other flights (-> Gwendal Rivière)
- Use other convection schemes (new PCMT, Tiedke)

Vertical profile of mean heating and $P\dot{V}$ along WCB trajectories

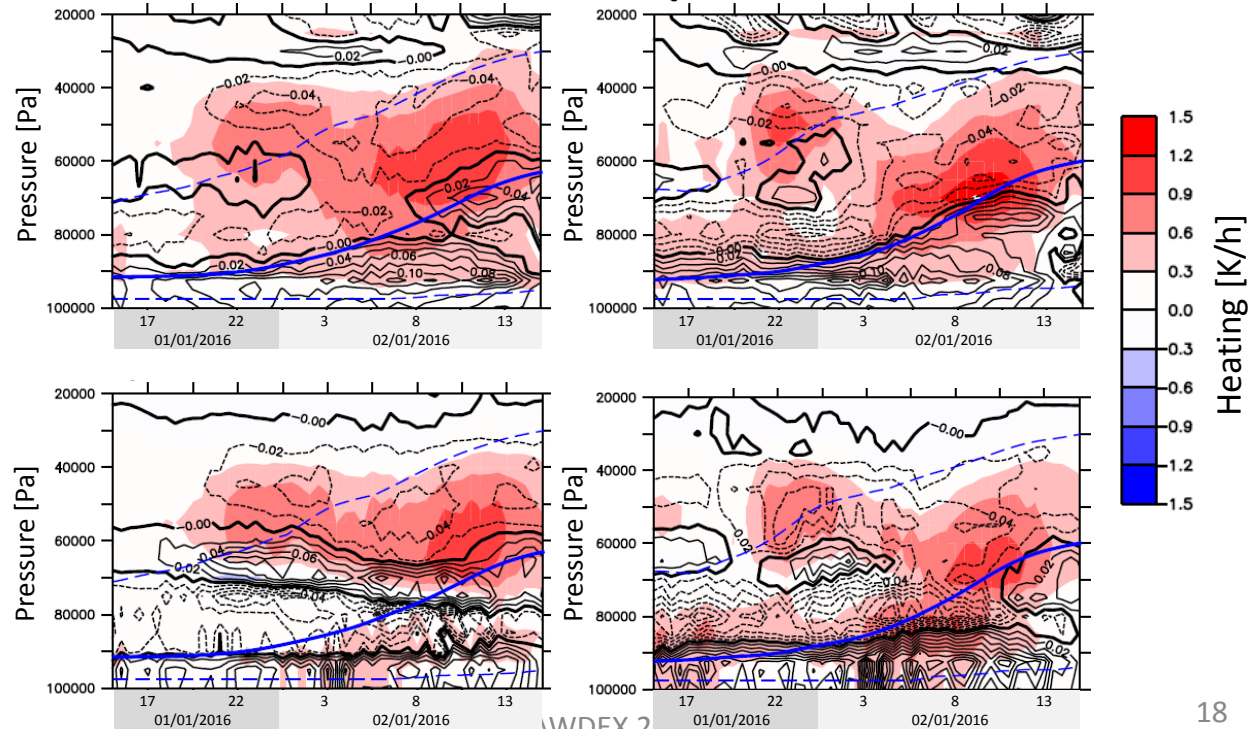
Finite differences

$$\frac{\theta(t + 15mn) - \theta(t - 15mn)}{\Delta t} + u \frac{\Delta \theta}{\Delta x} + v \frac{\Delta \theta}{\Delta y} + \omega \frac{\Delta \theta}{\Delta P}$$

$\dot{\theta}$ from DDH

B85

PCMT

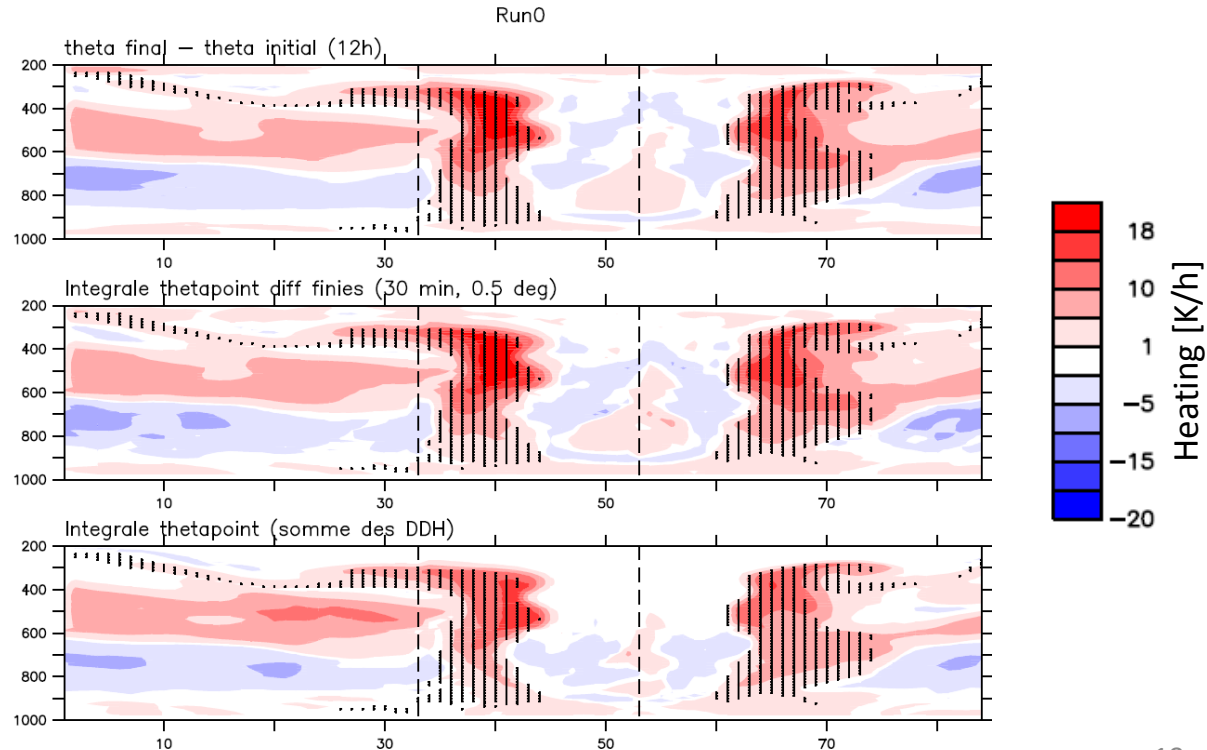


Integrated heating during 12h before the flight

Finite differences

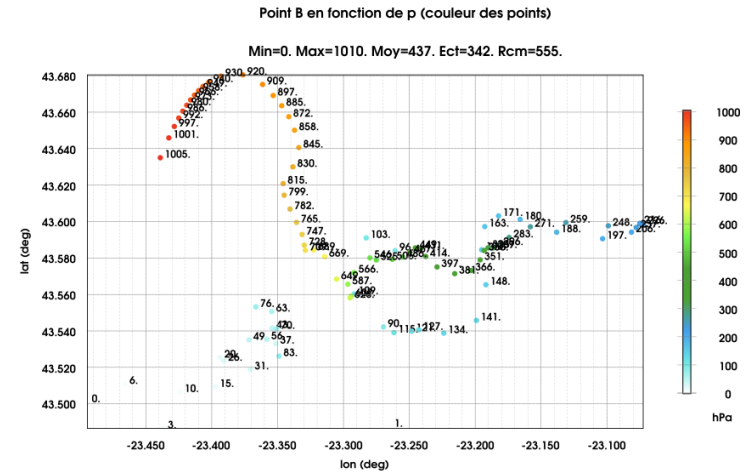
$$\int \left(\frac{\theta(t + 15mn) - \theta(t - 15mn)}{\Delta t} + u \frac{\Delta \theta}{\Delta x} + v \frac{\Delta \theta}{\Delta y} + \omega \frac{\Delta \theta}{\Delta P} \right) dt$$

$\int \dot{\theta} dt$ from DDH



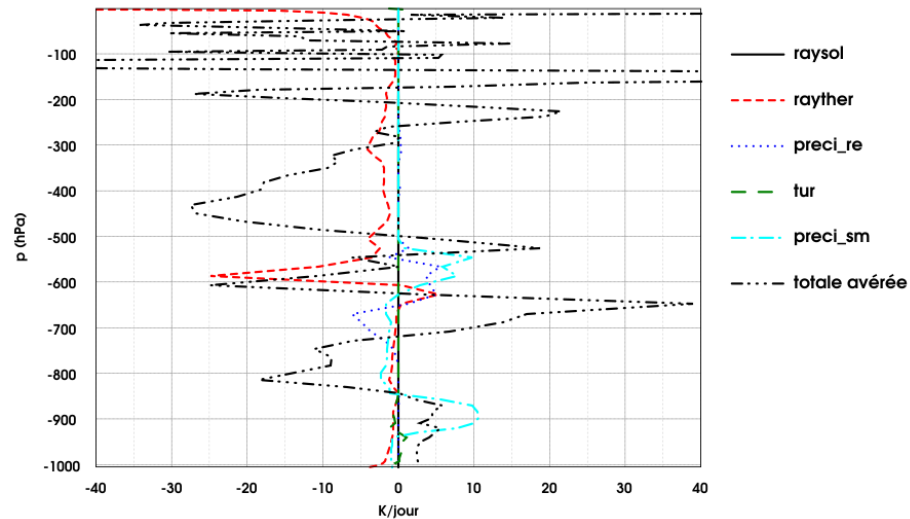


Thank you for your
attention



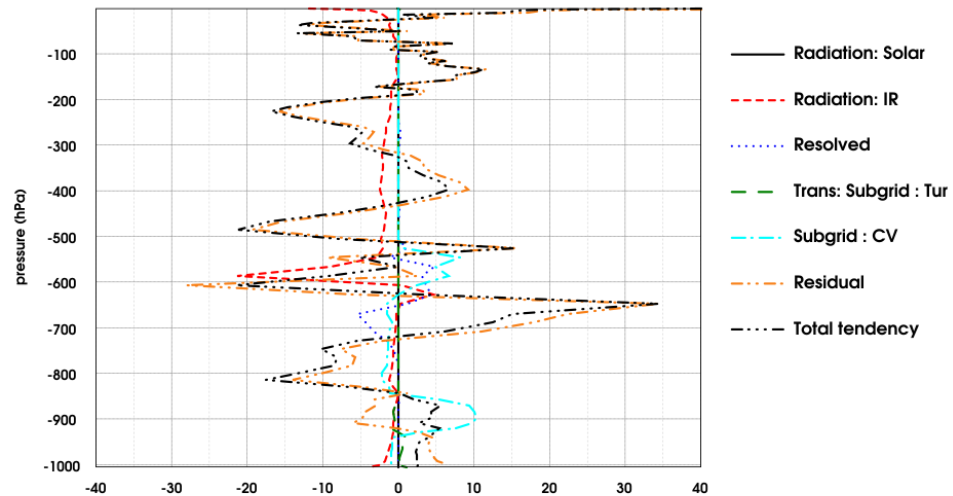
Tendance de theta en 15 mn, (lon,lat)=(-23.26692712,43.27491477)

DHFDLARPE+0076.ren.manq >>> DHFDLARPE+0078.ren.manq



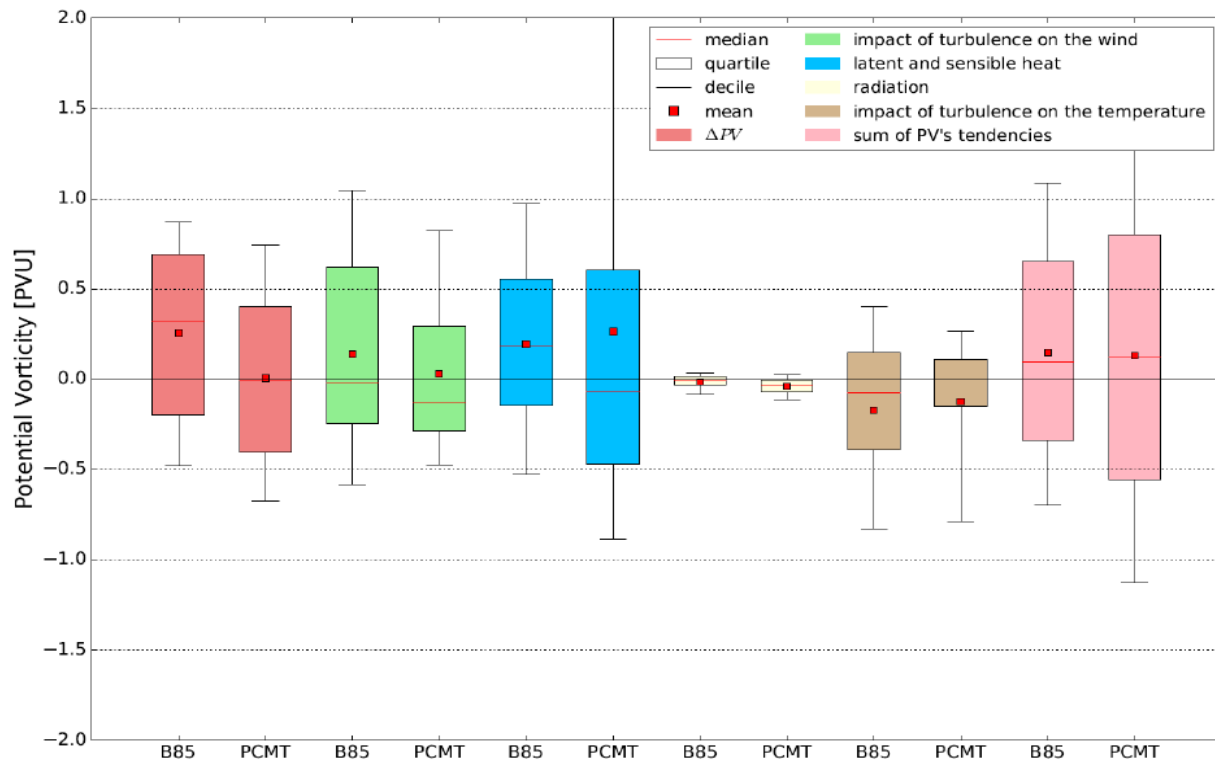
TEMPERATURE BUDGET (K/day) , FCST (fdiff2.lfa)

BASE 2016-10-01 21:30 ECH 0.25 H, 1 dom., 90 niv.



PV budget

12h before the flight, common WCB trajectories



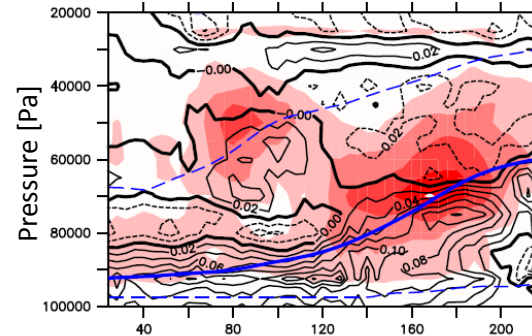
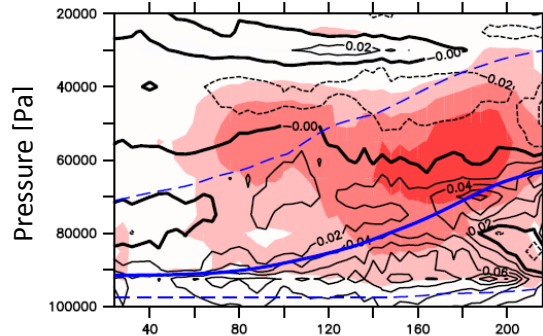
Vertical profile of mean heating and $P\dot{V}$ along S2 WCB trajectories

$$P\dot{V} = -g \left(- \frac{\partial \theta}{\partial P} \Big|_P (f + \xi) \right)$$

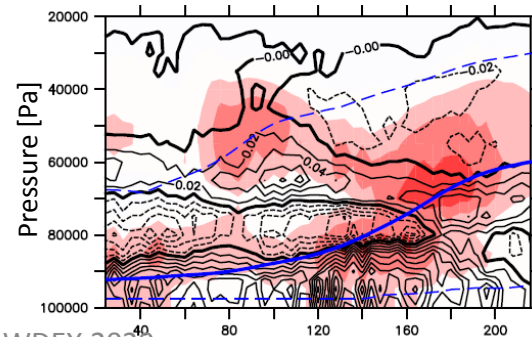
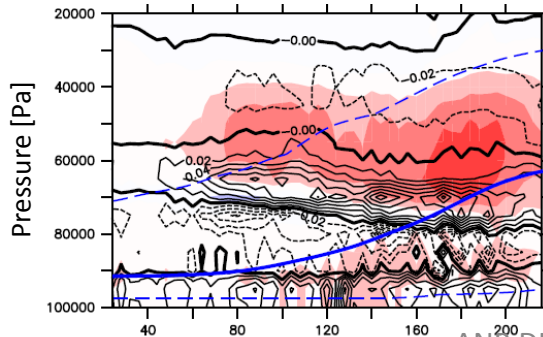
B85

PCMT

$$\frac{\partial \theta_{GRIB}}{\partial t}$$



$$\frac{\partial \theta_{DDH}}{\partial t}$$

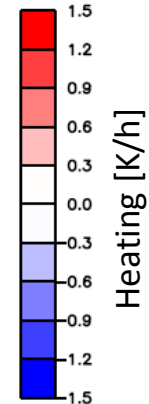
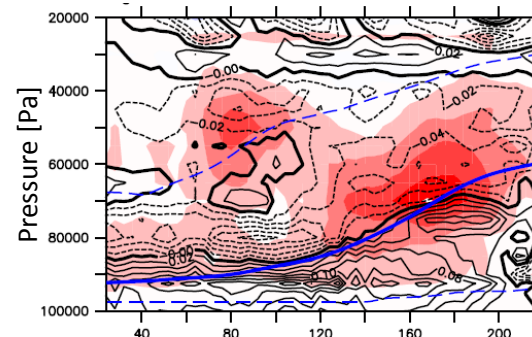
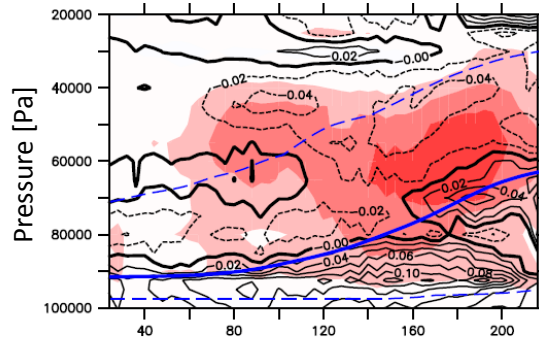


Vertical profile of mean heating and PV along S2 WCB trajectories

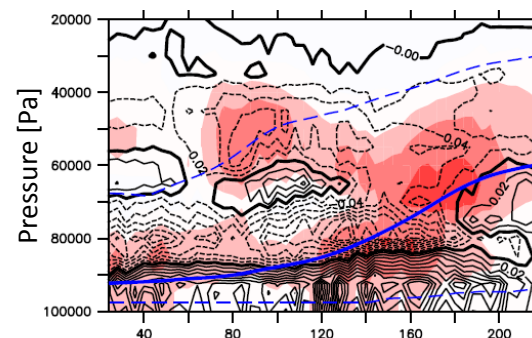
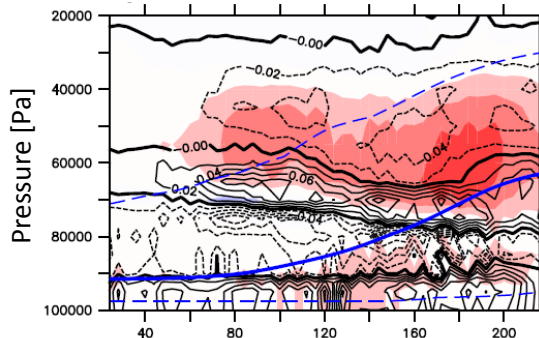
B85

PCMT

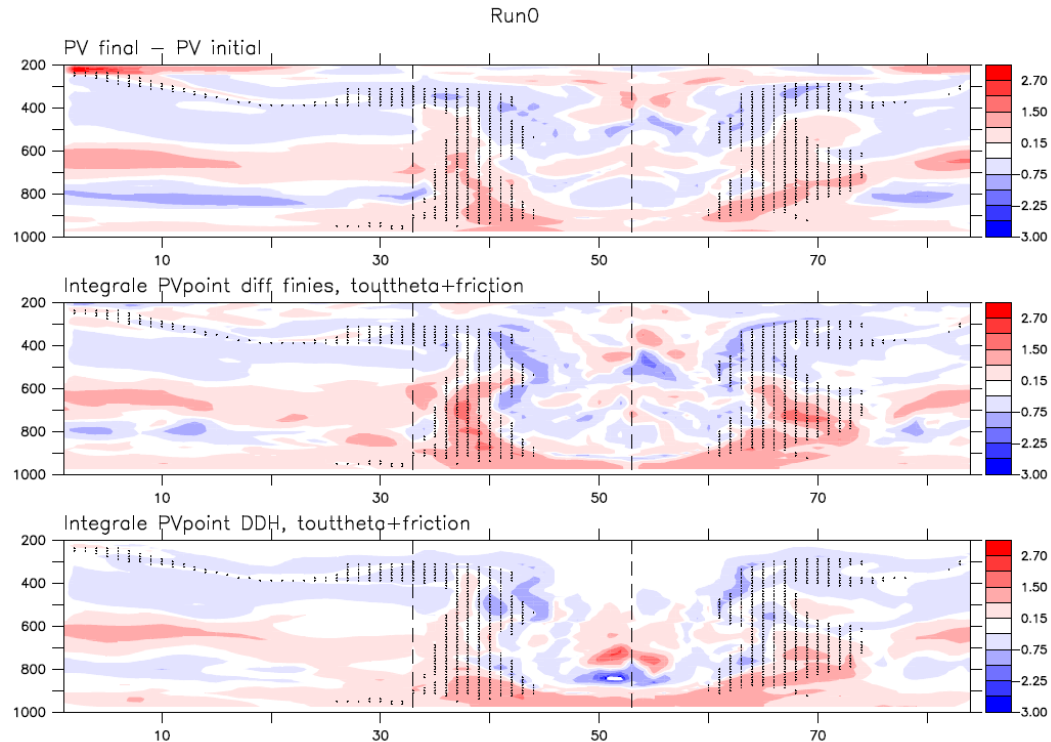
$$\frac{\partial \theta_{GRIB}}{\partial t}$$



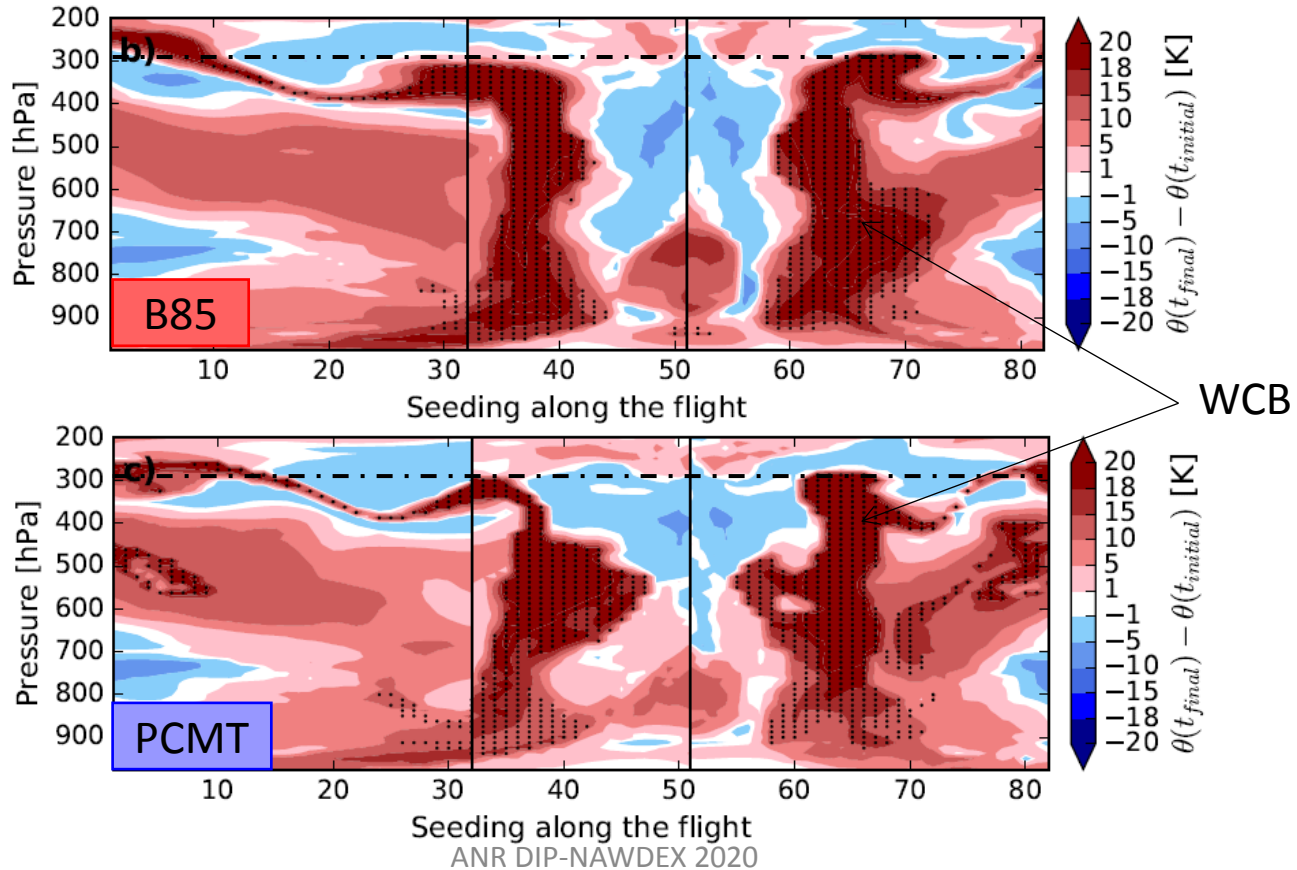
$$\frac{\partial \theta_{DDH}}{\partial t}$$



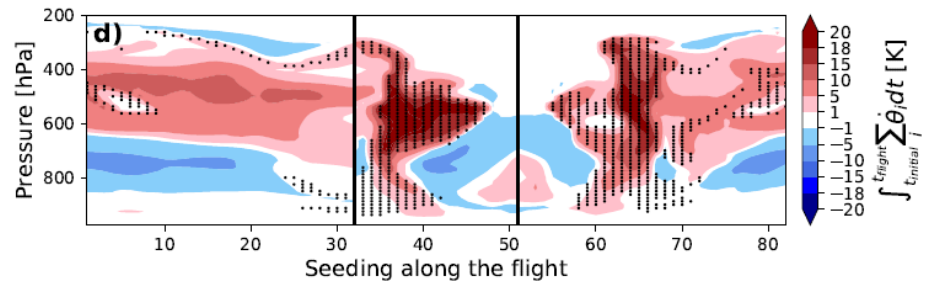
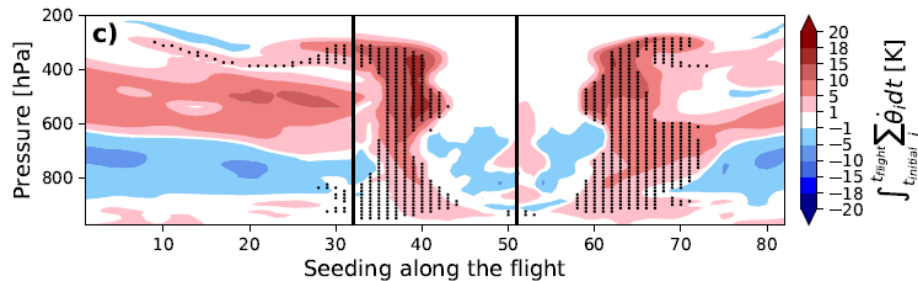
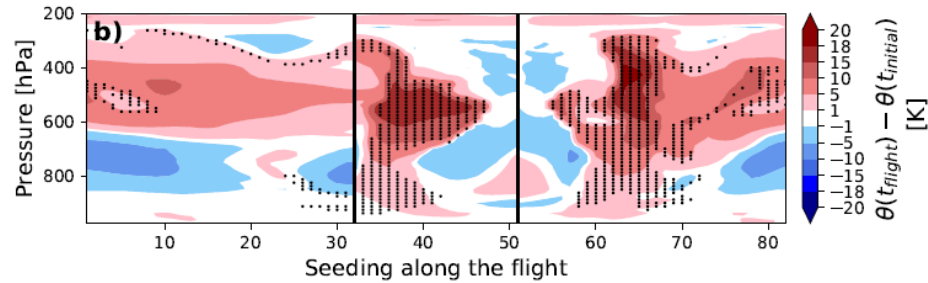
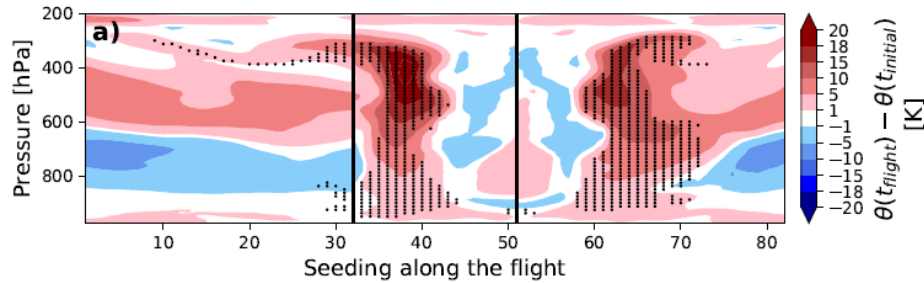
Integrated PV during the entire trajectories



Integrated heating along the total length of trajectories

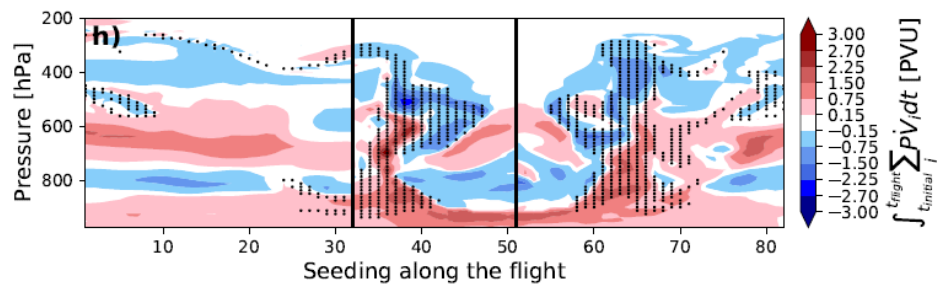
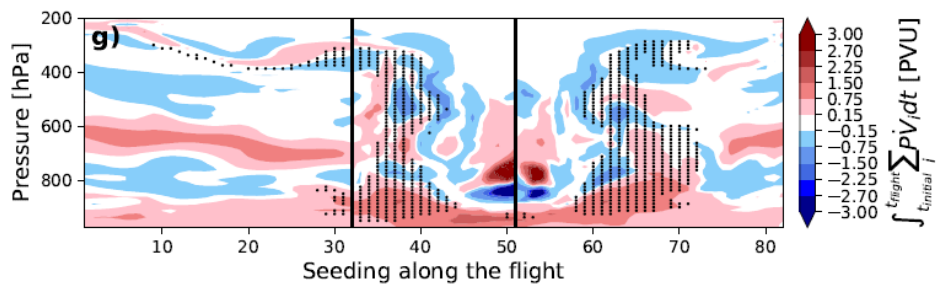
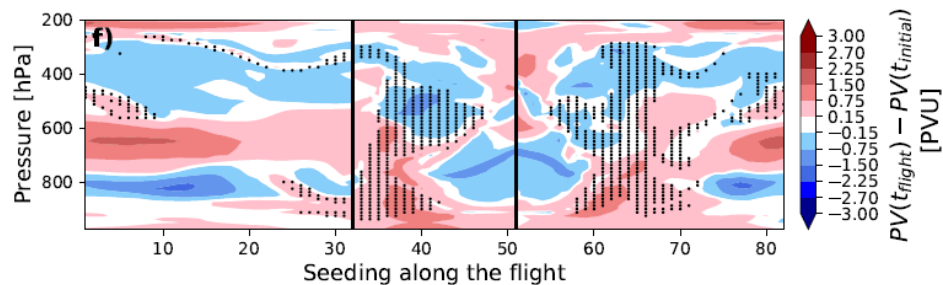
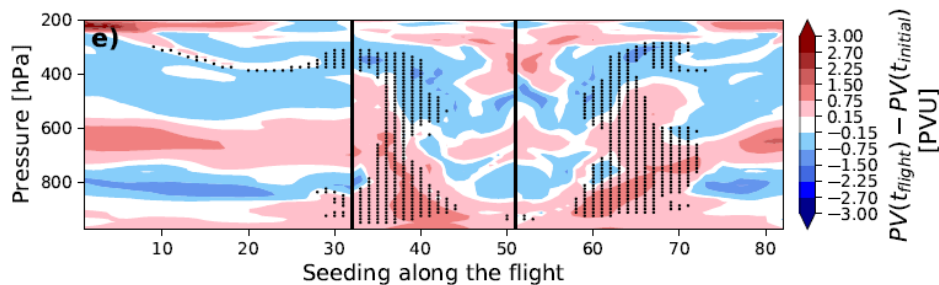


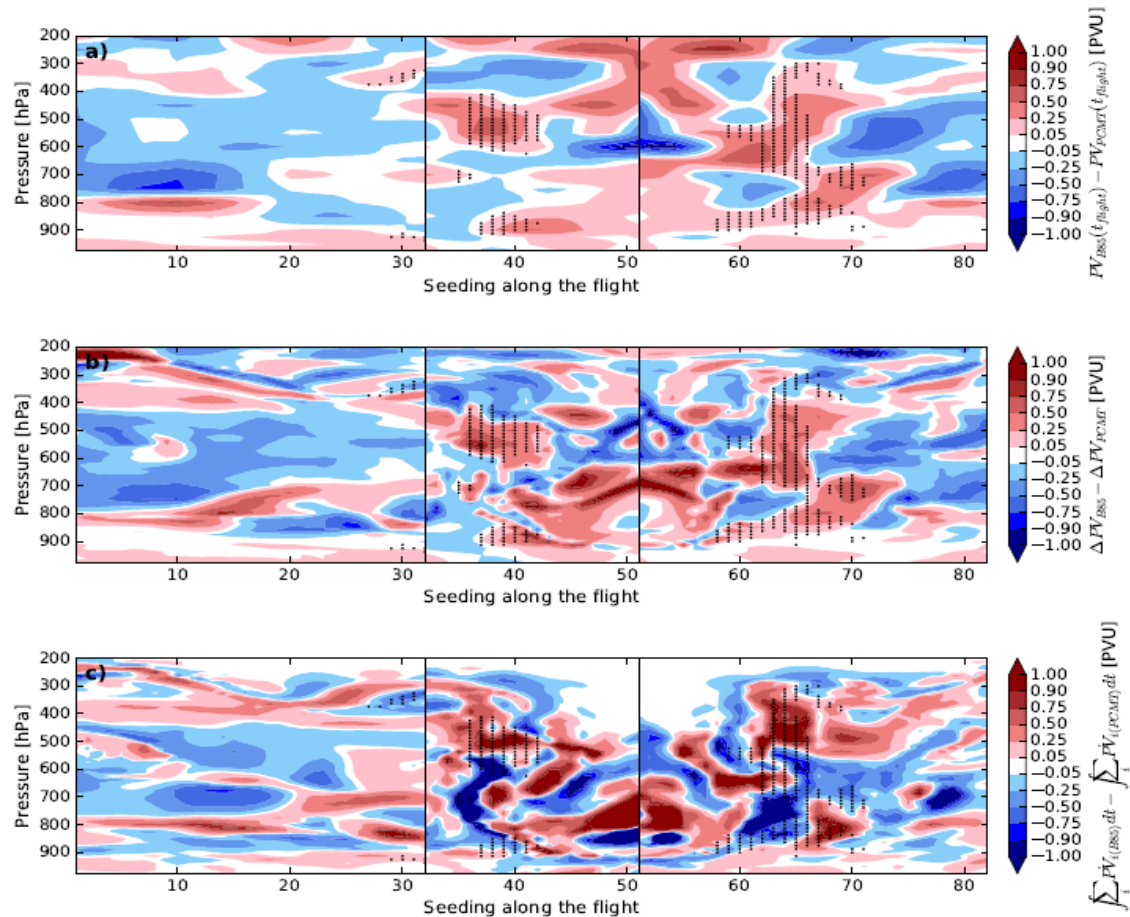
Heating budget 12h before the flight



PV budget

12h before the flight





Number of trajectories > 315K

