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The impact of deep convection schemes of a global atmospheric model on the warm conveyor belt and jet stream of NAWDEX IOP6

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NAWDEX workshop: 8 March 2021

Main questions

- How different are Warm Conveyor Belts between runs with parametrized deep convection and without ?
- How do distinct deep convection schemes differ in the representation of WCBs ?
- What is the impact of parametrized convection on jet stream in the WCB outflow region ?
- What are the forecast errors in the representation of the jet stream for the different runs with and without parametrized convection ?

Model and set up of the simulations

Model: global operational model Arpege

- Model resolution: T798 with stretching → 10km over France, 20km on Iceland
- Output resolution: lon x lat: 0.5° x 0.5°
- 3 simulations differing only on deep convection representation

Bougeault, 1985

B85

- Mass-flux scheme
 - Closure in humidity
-  used in operational NWP version

Piriou et al, 2007

PCMT

- Mass-flux scheme
- Closure in CAPE
- Linked to microphysics and transport schemes
- Strong entrainment

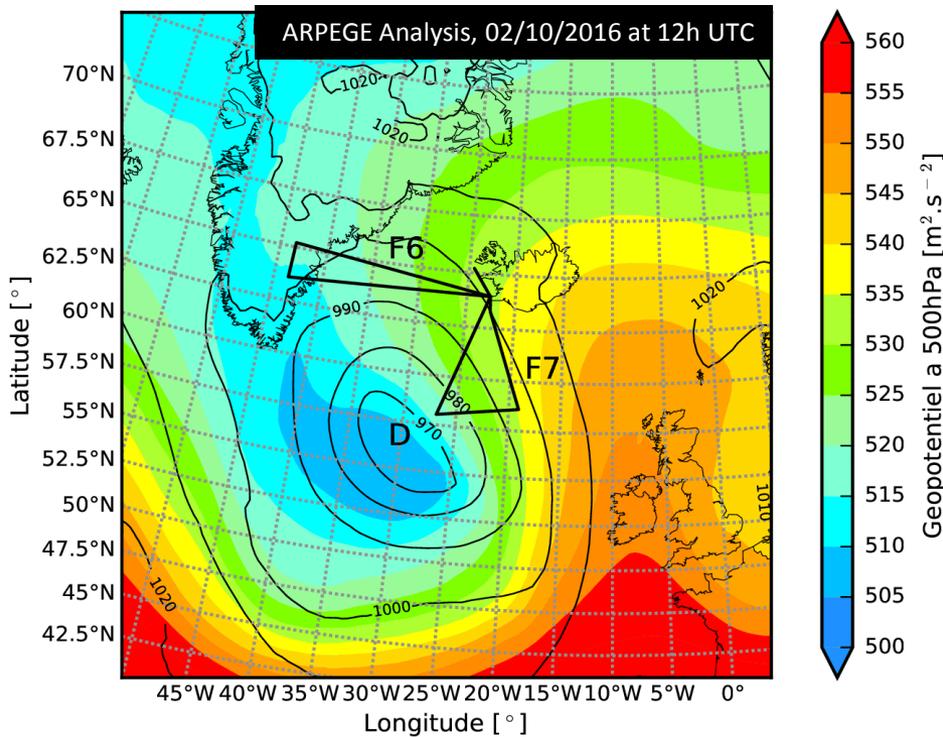
 used in ARPEGE-CLIMAT

No parametrized deep convection

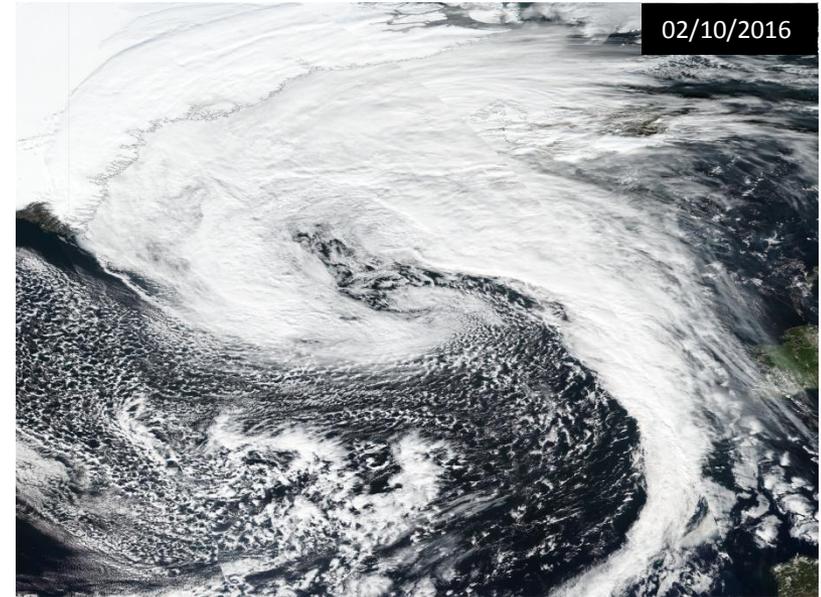
NoConv

Case study: IOP6 – Stalactite Cyclone

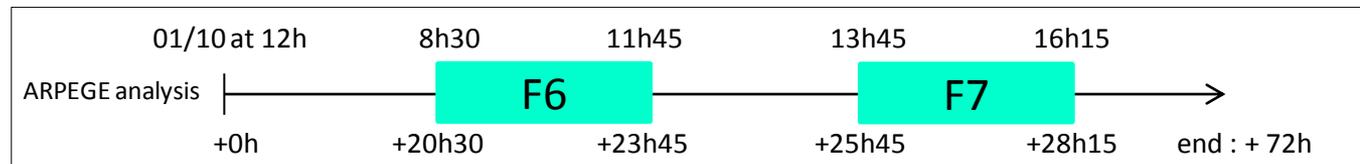
Geop 500 hPa (shadings) SLP (contour)



MODIS, Nasa Worldview Application



Timing of the runs vs flights:



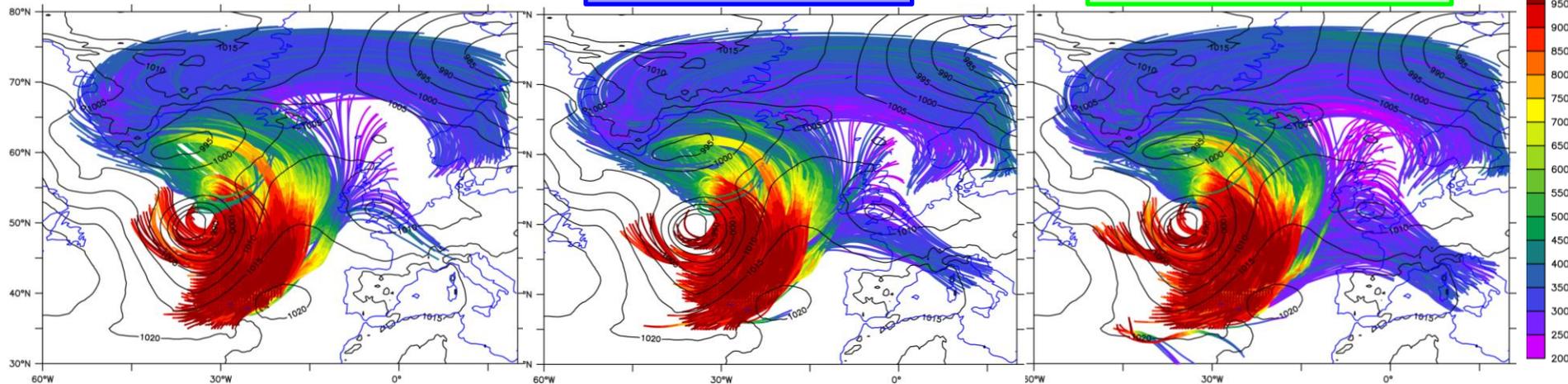
Computation of Lagrangian trajectories

Computation of Lagrangian trajectories starting in the warm sector at the
initial time: 12h UTC 1 October
Criterion : if exceeds 300 hPa ascents within 24h

B85: 9 876 traj

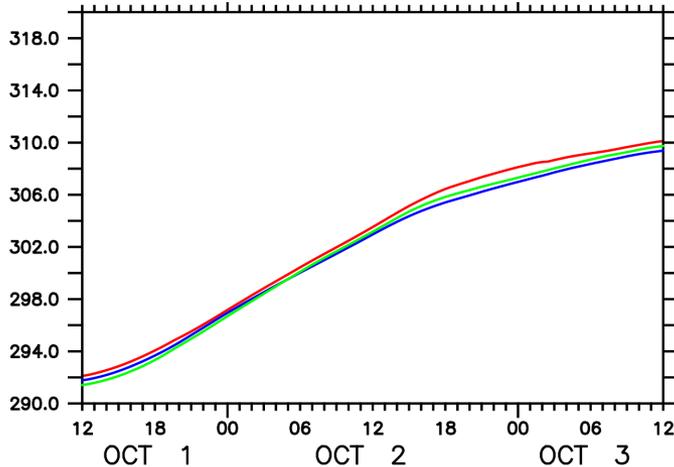
PCMT: 10 086 traj

NoConv: 11 421 traj

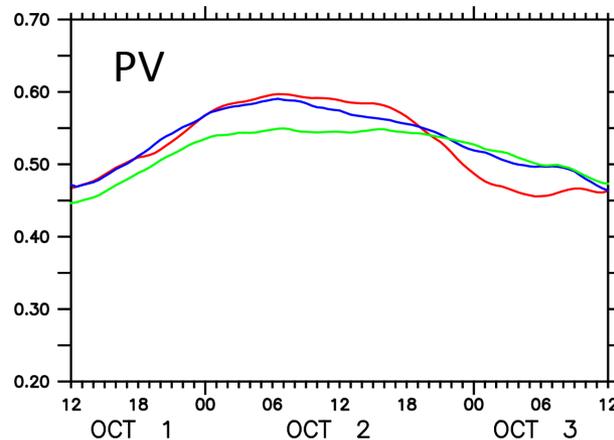
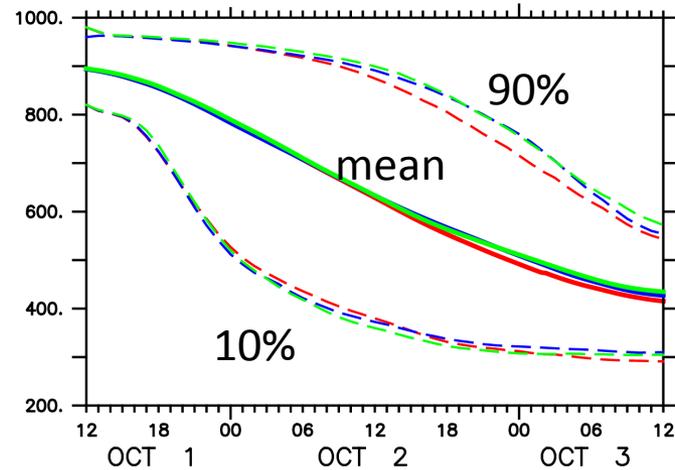


Averaged quantities along trajectories

Potential temperature



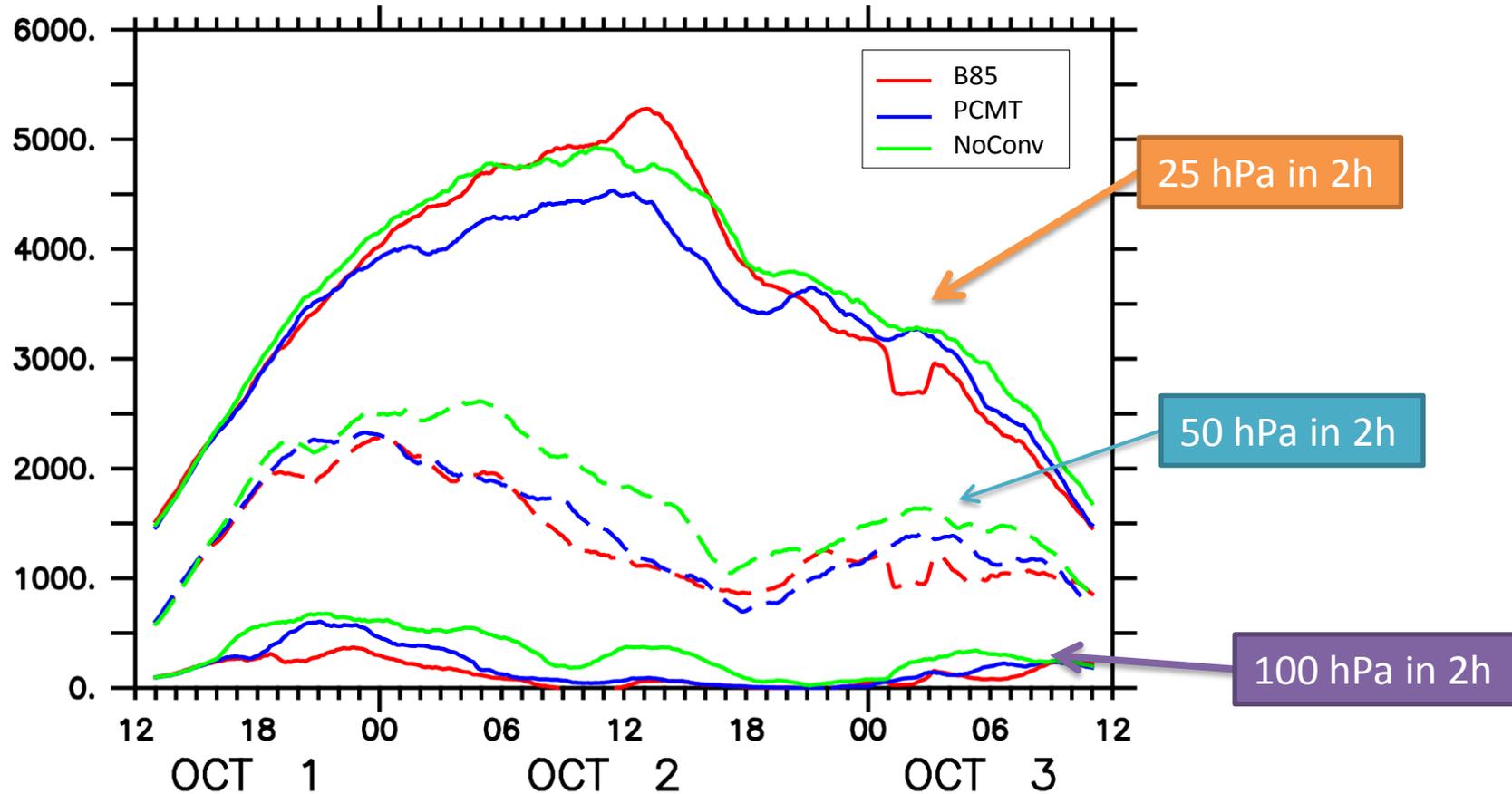
Pressure



— B85
— PCMT
— NoConv

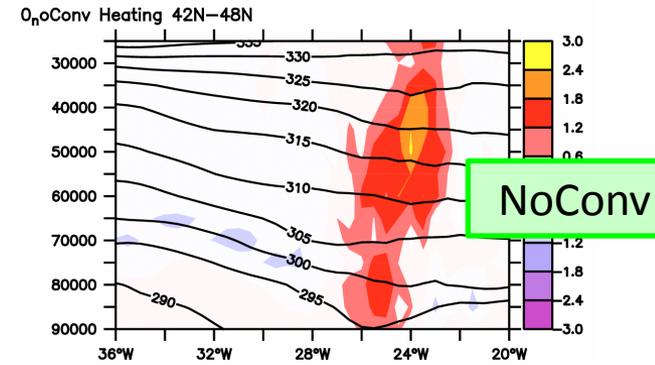
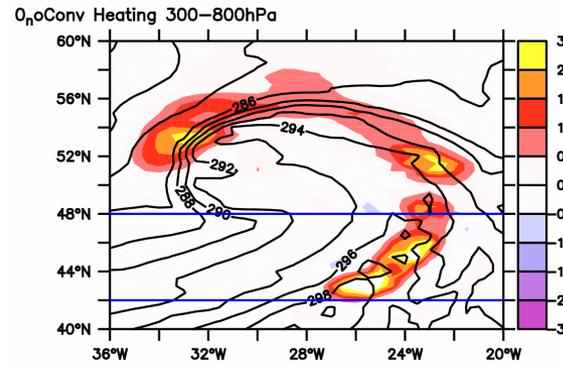
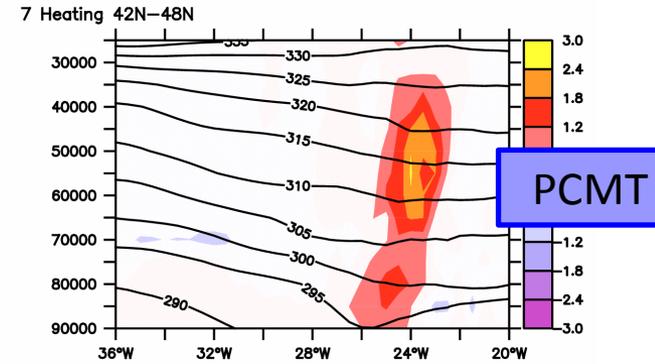
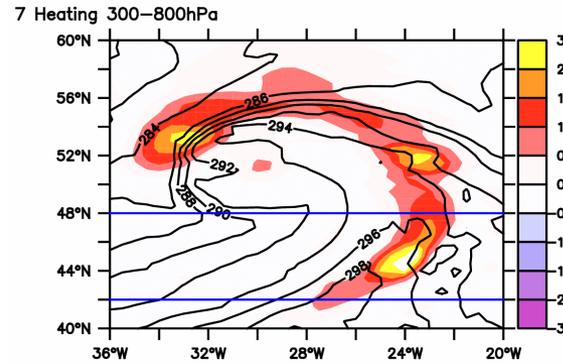
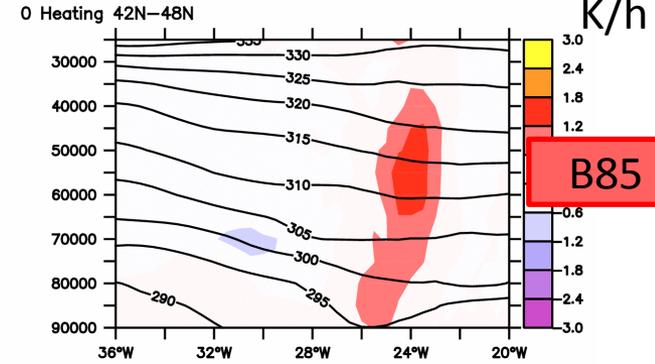
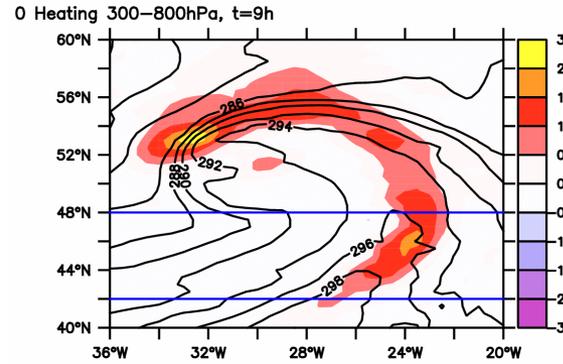
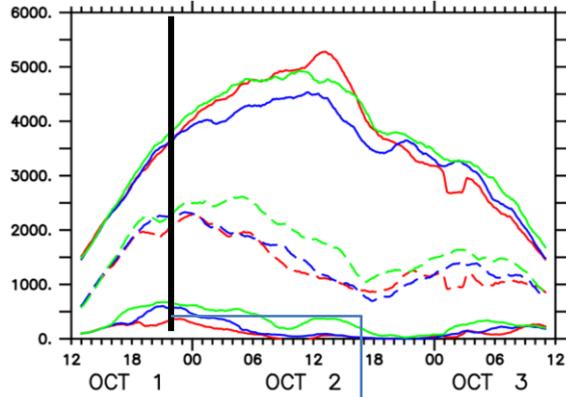
- Slightly more WCBs in NoConv than in runs with parametrized convection
- No drastic differences in the mean pressure or potential temperature
- PV shows more differences: B85 has a more important PV decrease at the end

Nber of trajectories satisfying a criterion on ascents



Fastest ascents for the run without convection scheme

Early times (t0+9h) and fast ascents (100 hPa/2h)



B85

PCMT

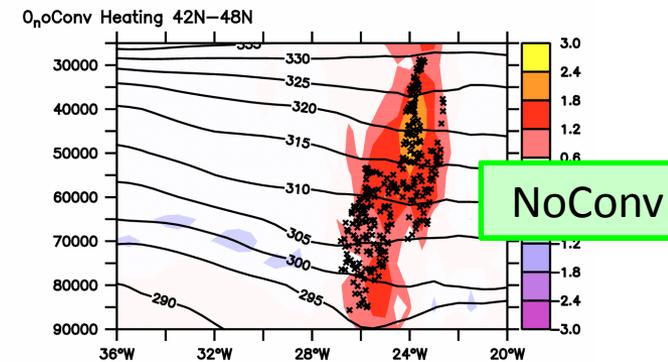
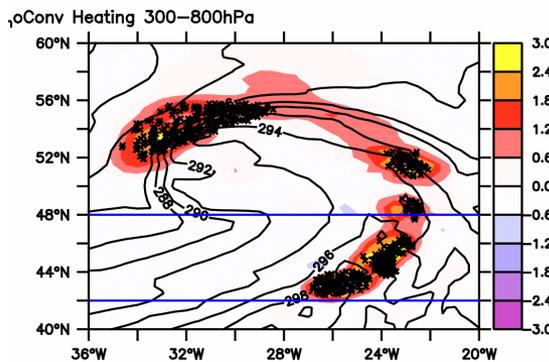
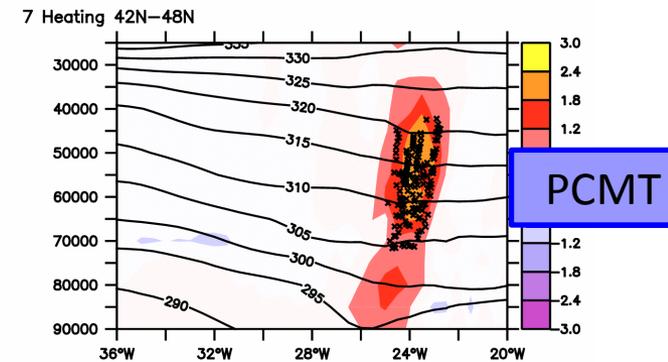
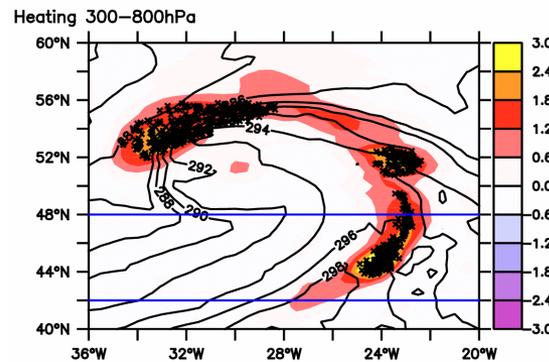
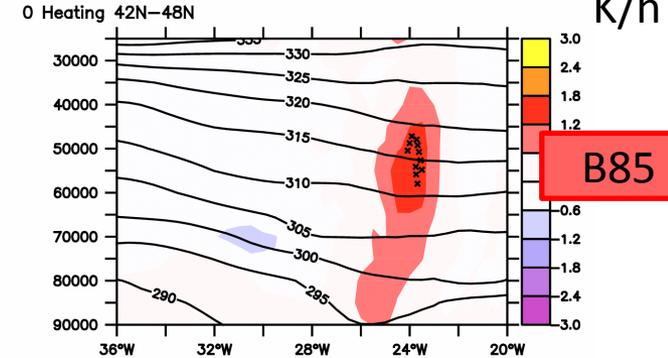
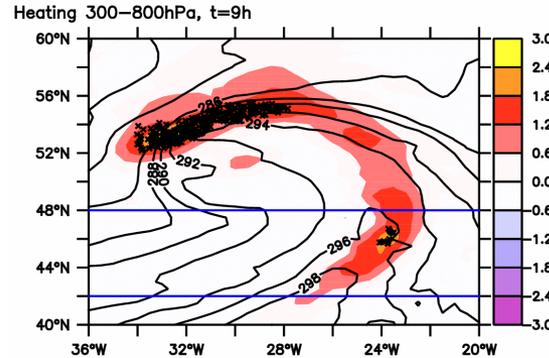
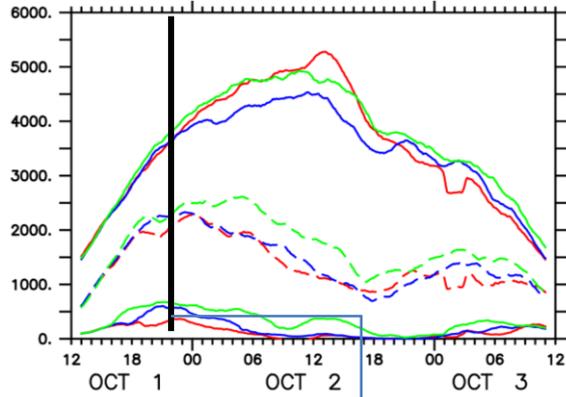
NoConv

Shadings: vertically averaged heating rate θ

Contours: 850-mb θ

Stronger, less homogeneous heating rate without convection scheme

Early times (t0+9h) and fast ascents (100 hPa/2h)



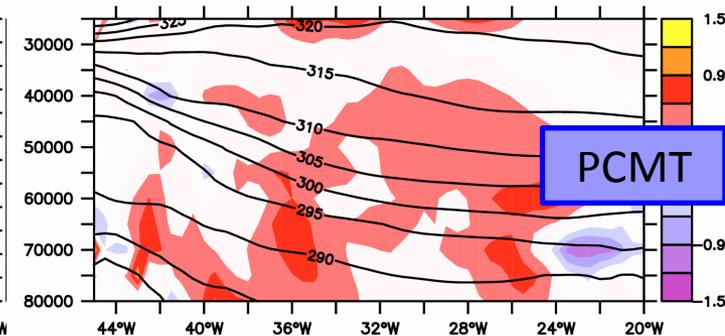
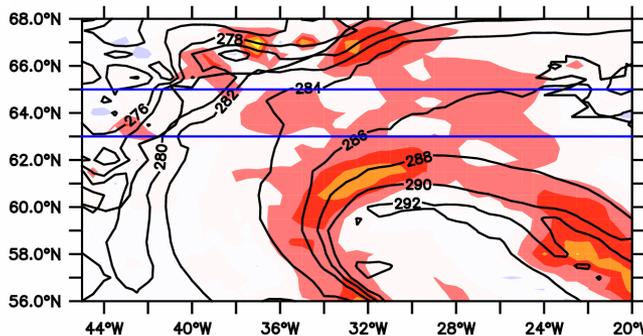
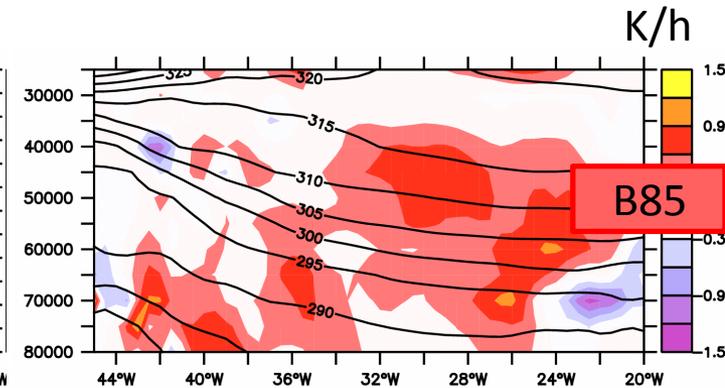
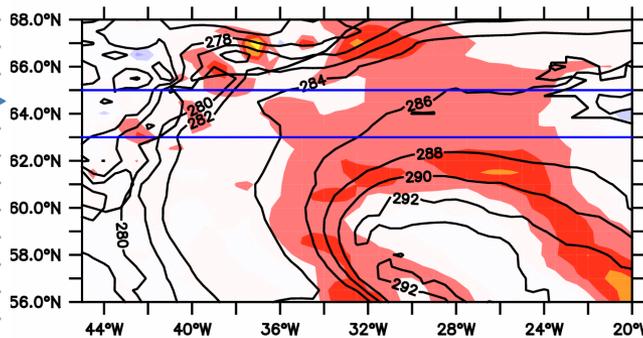
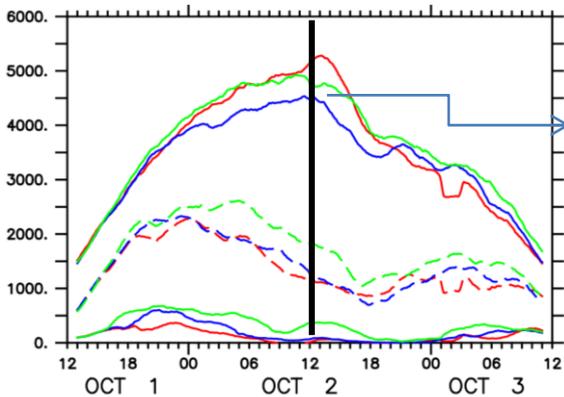
Shadings: vertically averaged heating rate $\dot{\theta}$

Contours: 850-mb θ

WCB with ascents 100hPa/2h

Stronger, less homogeneous heating rate without convection scheme

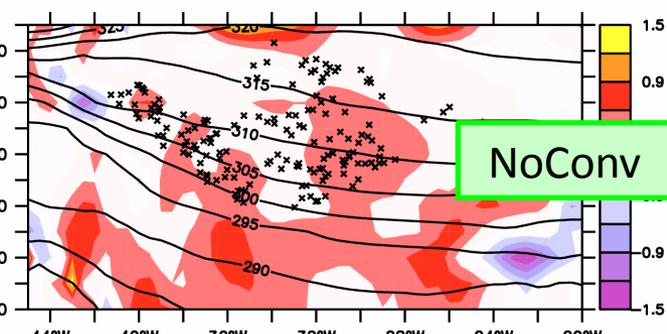
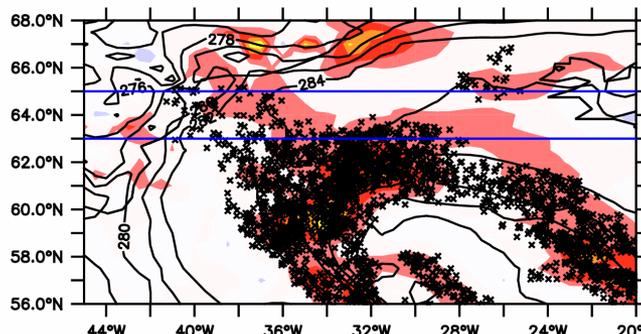
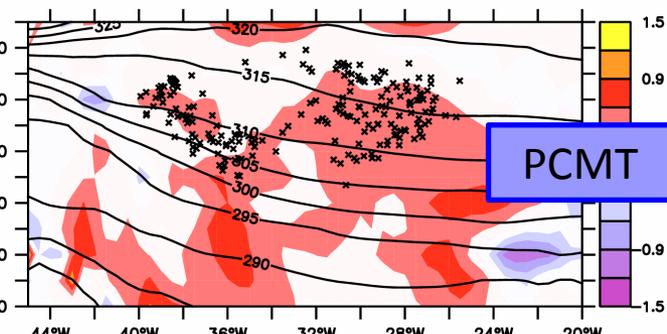
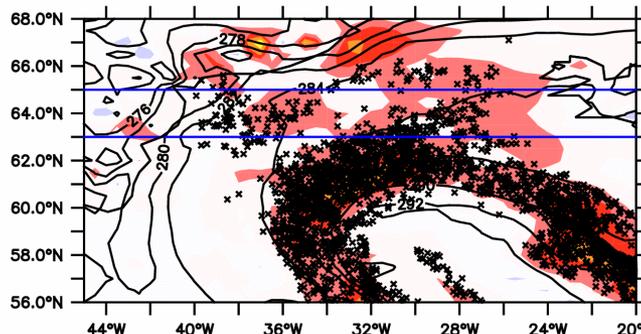
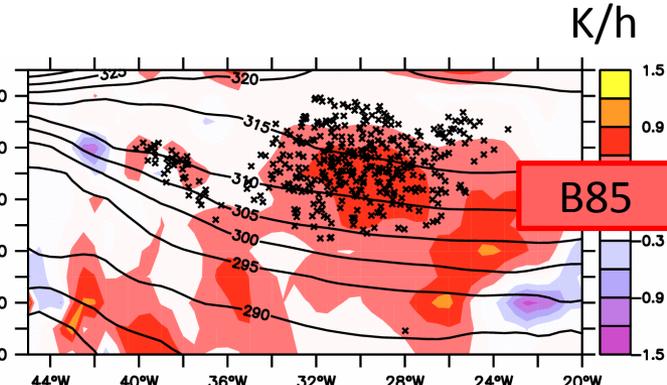
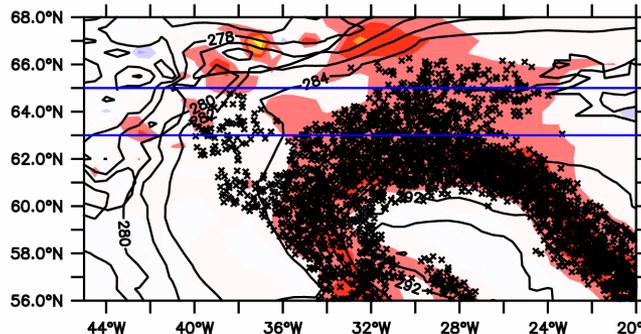
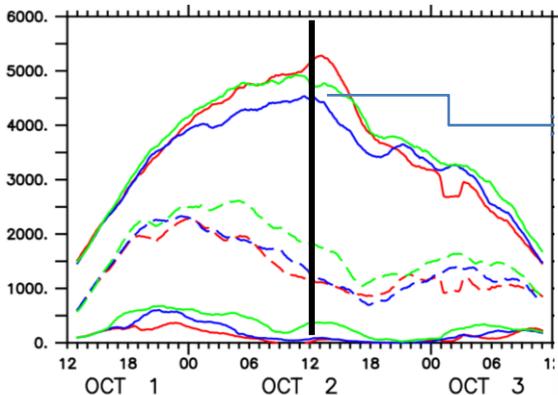
Later times (t0+24h) and moderate ascents (25 hPa/2h)



Shadings: vertically averaged heating rate $\dot{\theta}$

Contours: 850-mb θ

Later times (t0+24h) and moderate ascents (25 hPa/2h)

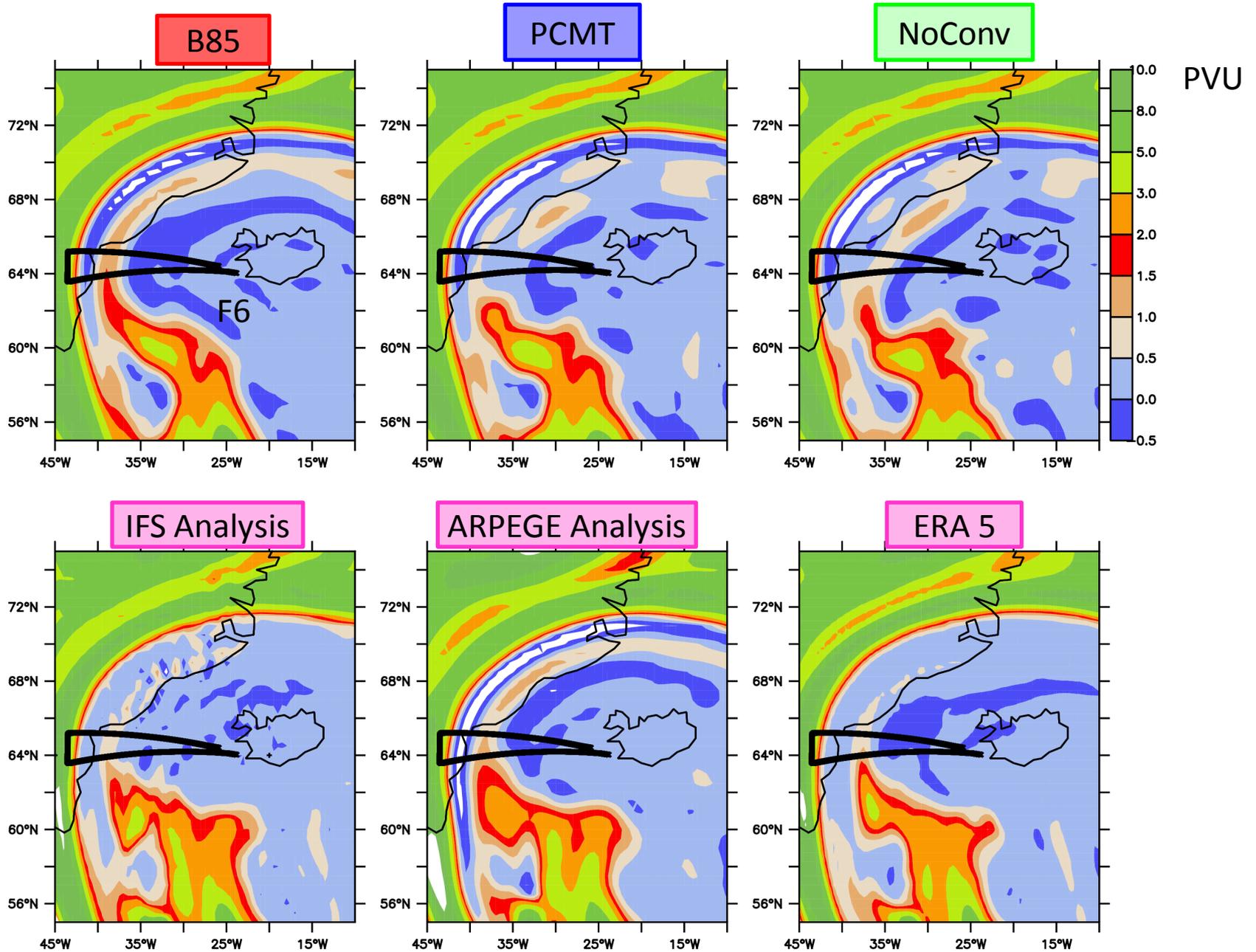


Shadings: vertically averaged heating rate $\dot{\theta}$

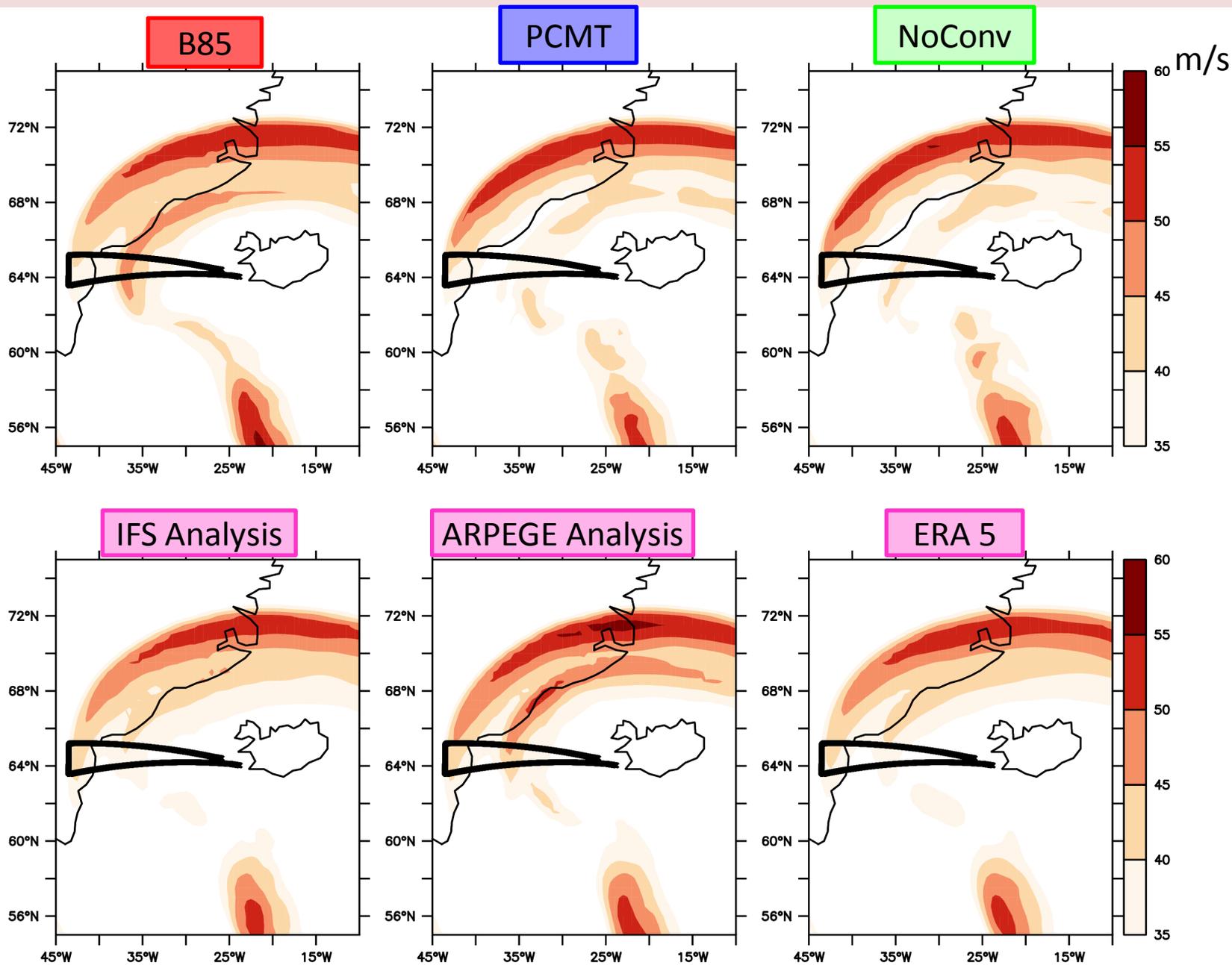
Contours: 850-mb θ

WCB: 25hPa/2h

PV anomalies at 300 hPa at t=24h



Wind speed at 300 hPa at t=24h



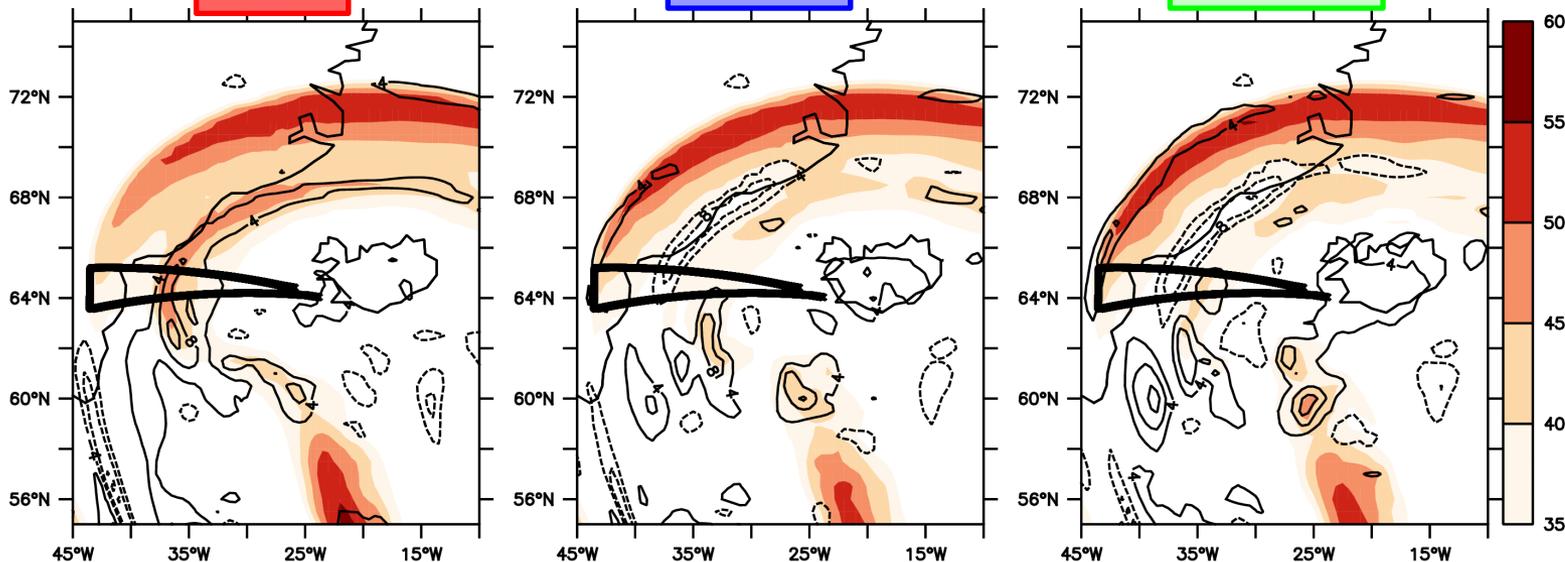
Wind speed at 300 hPa at t=24h

B85

PCMT

NoConv

m/s

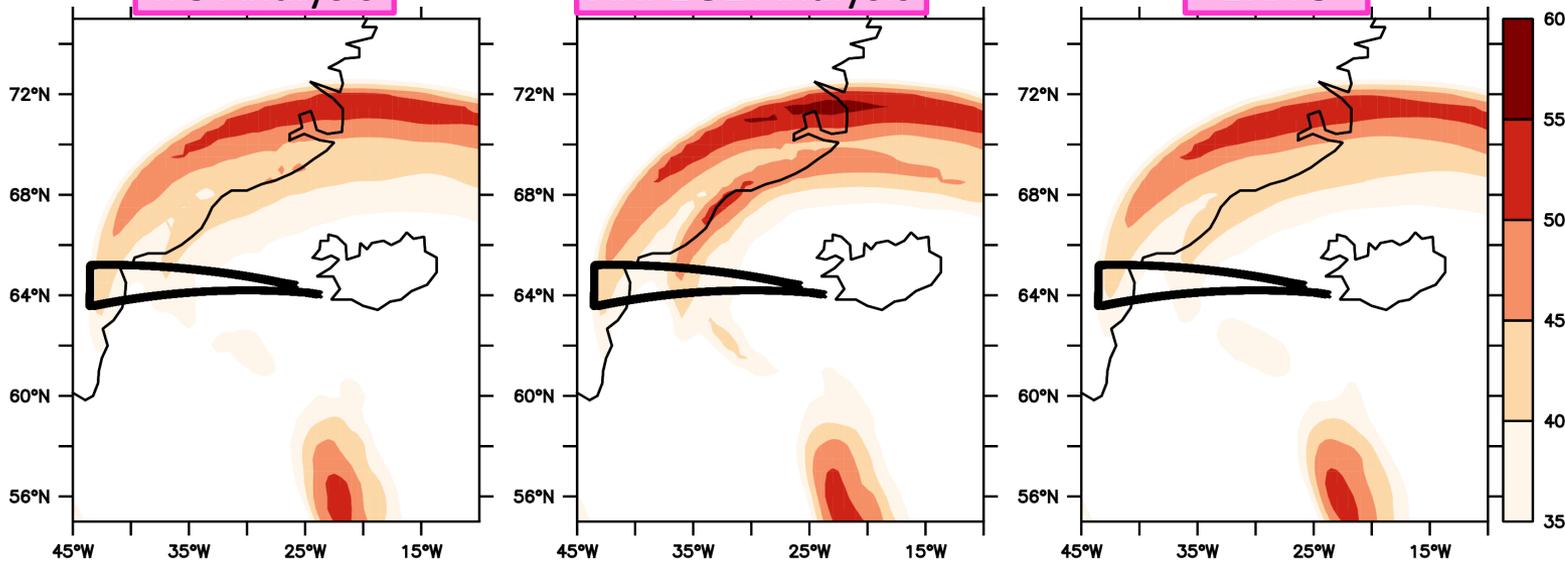


Contours:
difference
with IFS

IFS Analysis

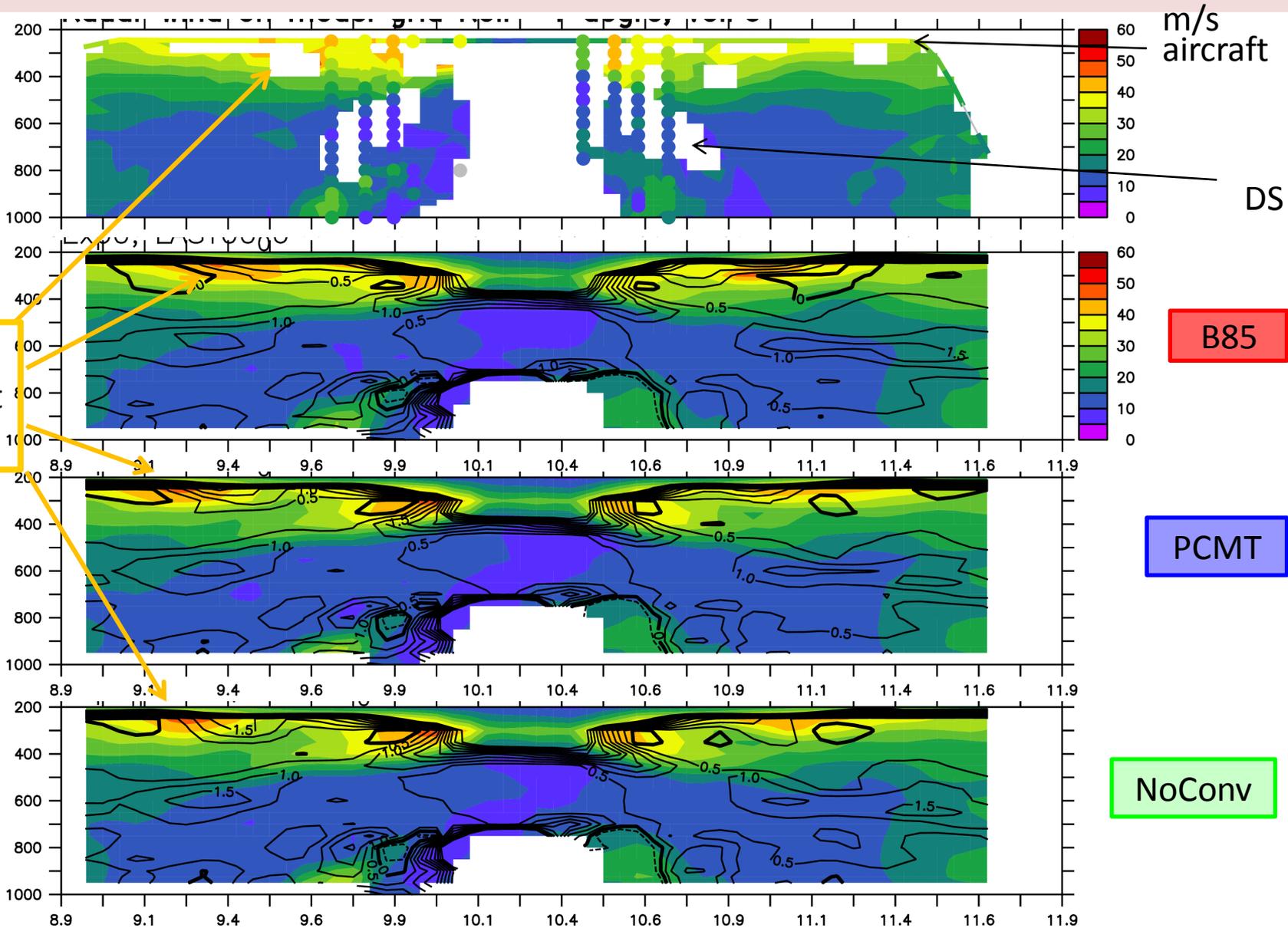
ARPEGE Analysis

ERA 5



Wind speed vertical profiles along Flight 6

Radar
RASTA
OBS



m/s
aircraft

DS

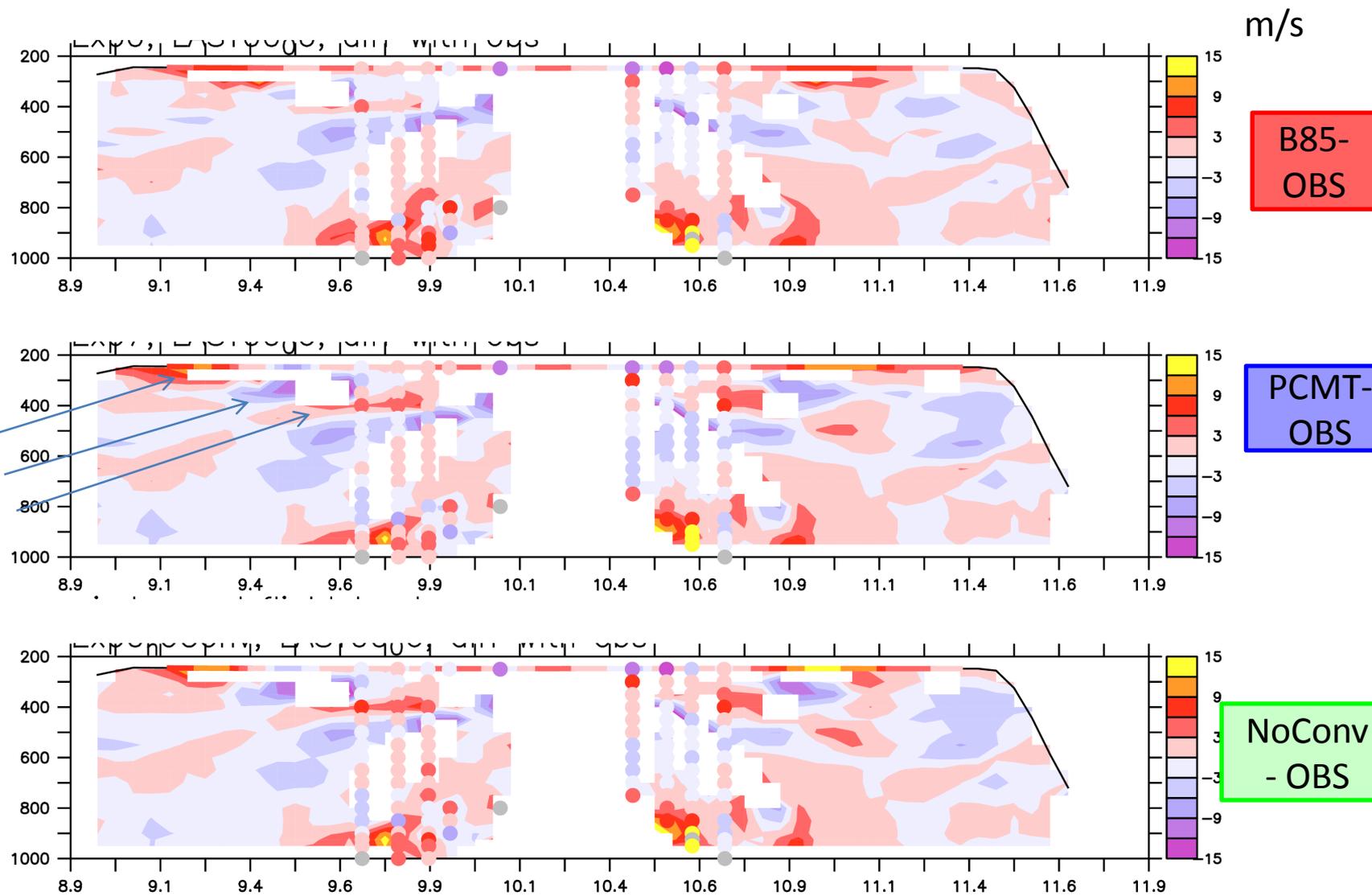
B85

PCMT

NoConv

See the
different jet
positions !

Wind speed anomalies with respect to observations

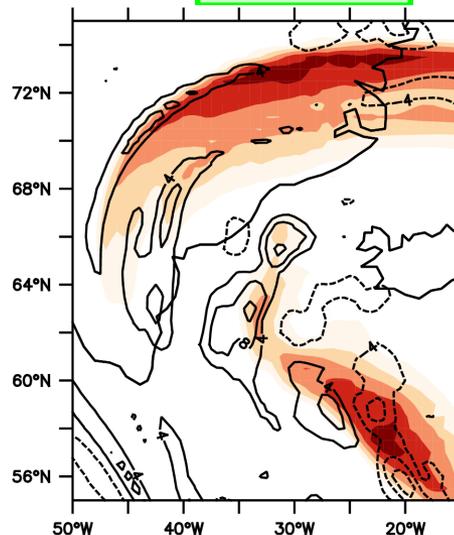
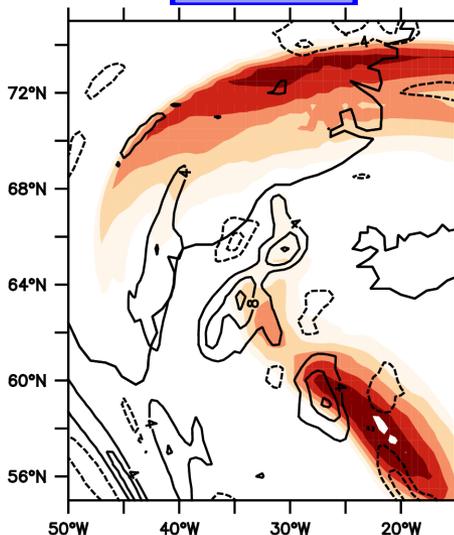
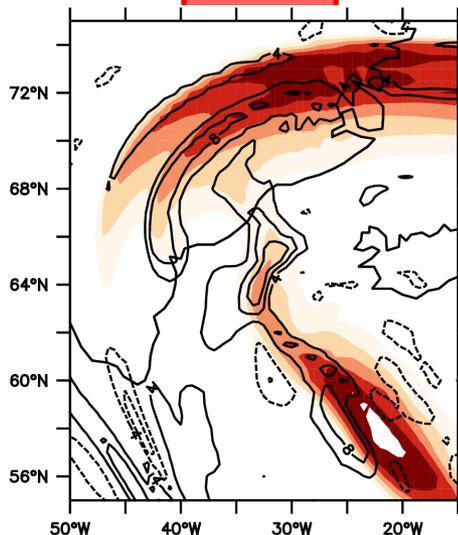


Wind speed forecast error after 30h

B85

PCMT

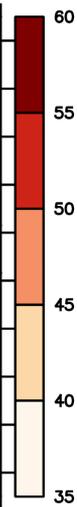
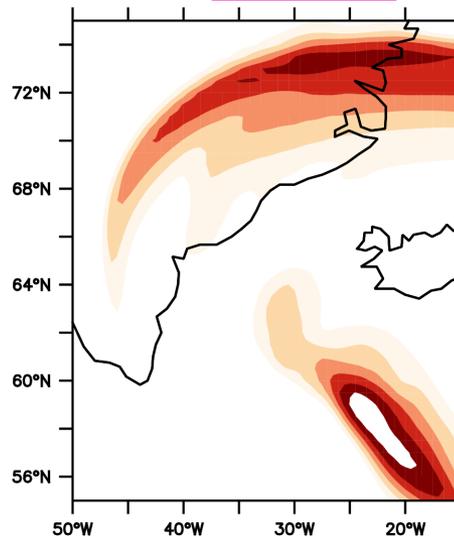
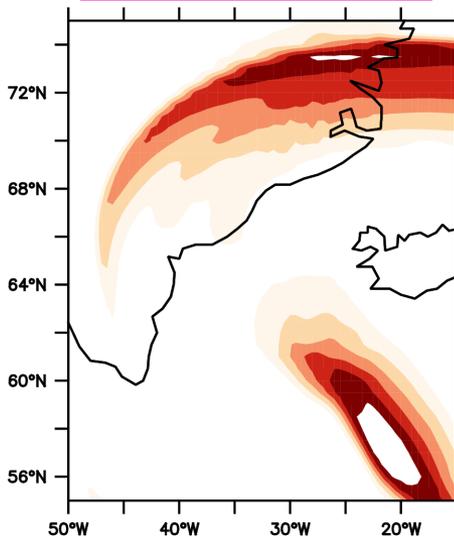
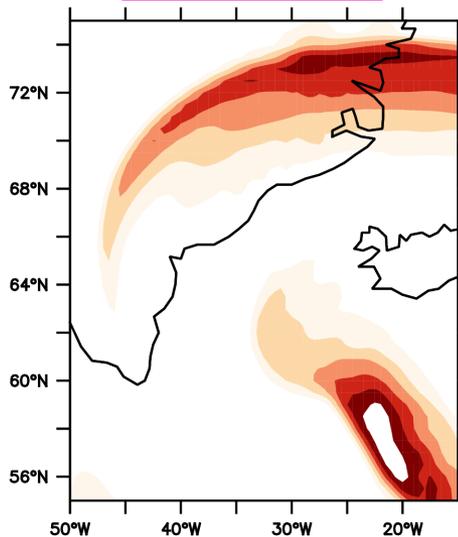
NoConv



IFS Analysis

ARPEGE Analysis

ERA 5



Contours:
difference
with IFS

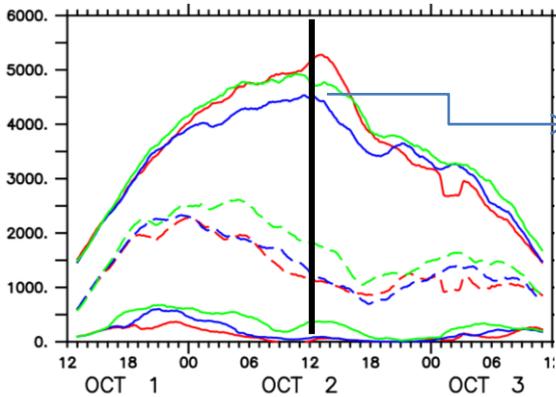
Conclusion

- **NoConv**: sooner stronger heating, more isolated regions, more rapid ascents than **B85** and **PCMT** ahead of the cold front
- More sustained ascents in **B85** than **PCMT** and **NoConv**
- **PCMT** has an intermediate behavior between **B85** and **NoConv**.
- More PV destruction in WCB outflow region in **B85** than **PCMT** and **NoConv**.
- The more active dynamics in the upper troposphere in **B85** is consistent with observations and (re)-analysis but too strong (consistent with IWC observations, not shown).

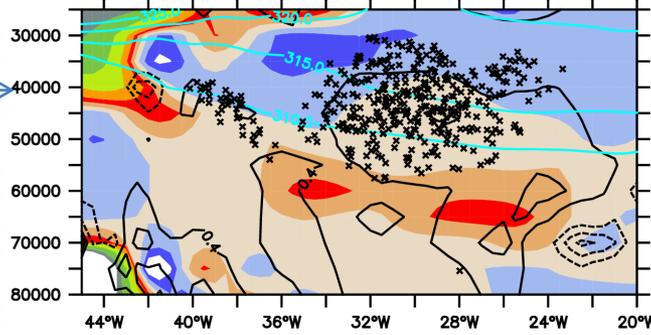
Outlook: Comparison with Tiedtke (1993) scheme used in IFS

Additional slides

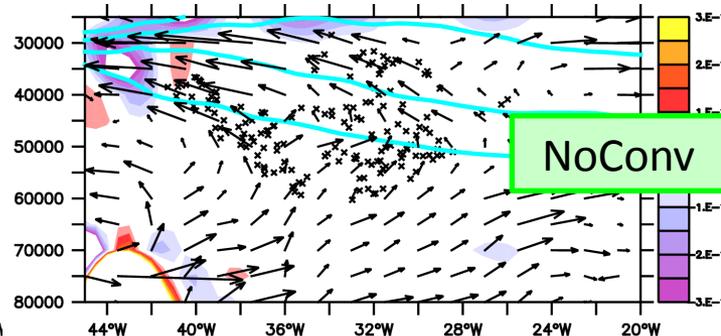
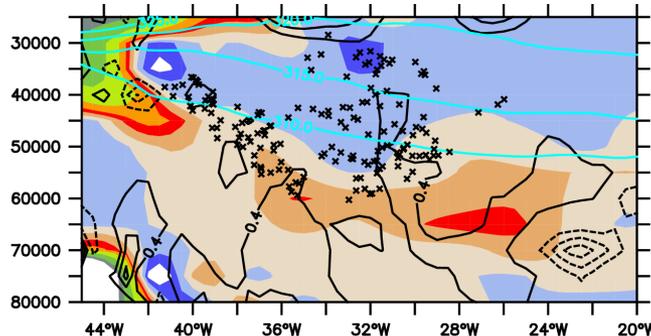
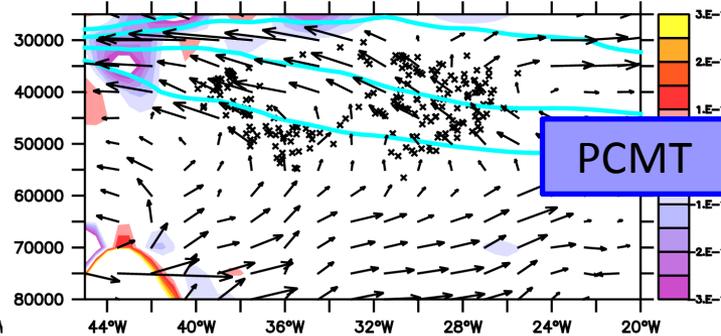
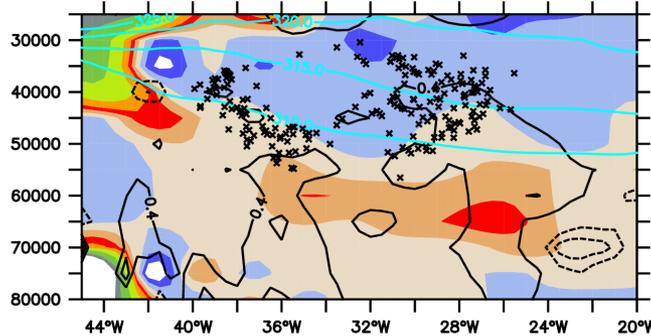
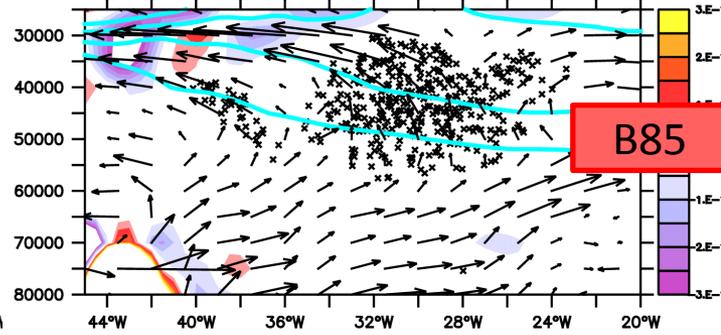
Later times (t0+24h)



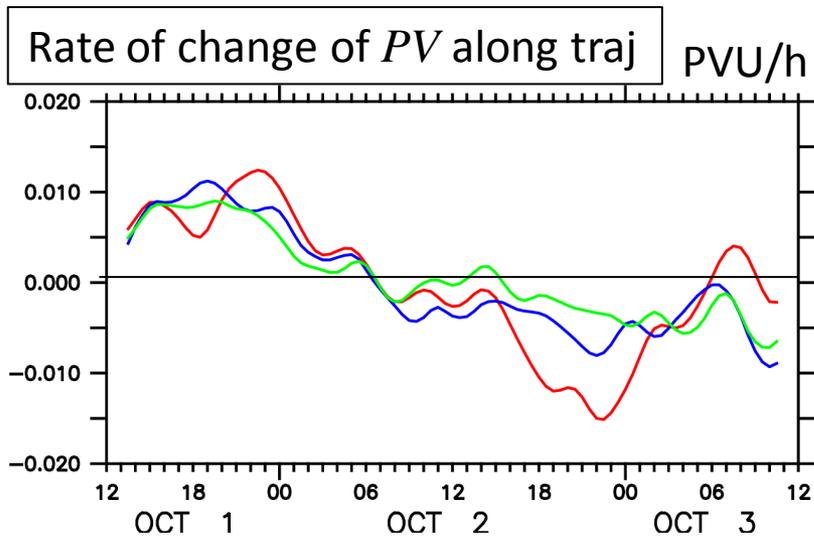
PV



Ageostrophic wind PV advection



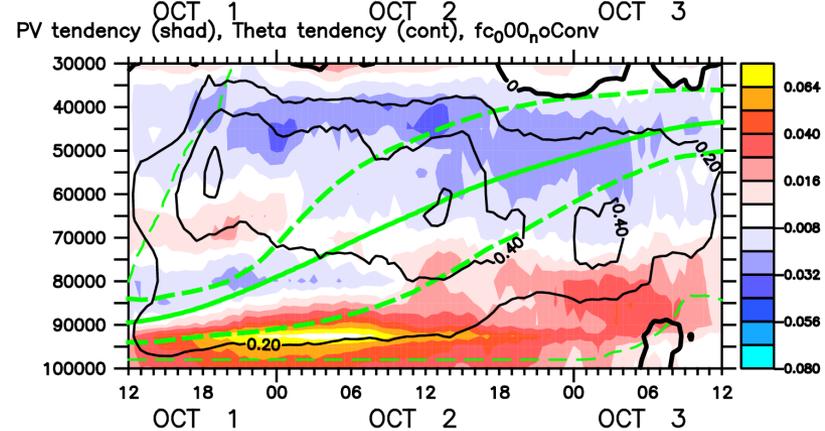
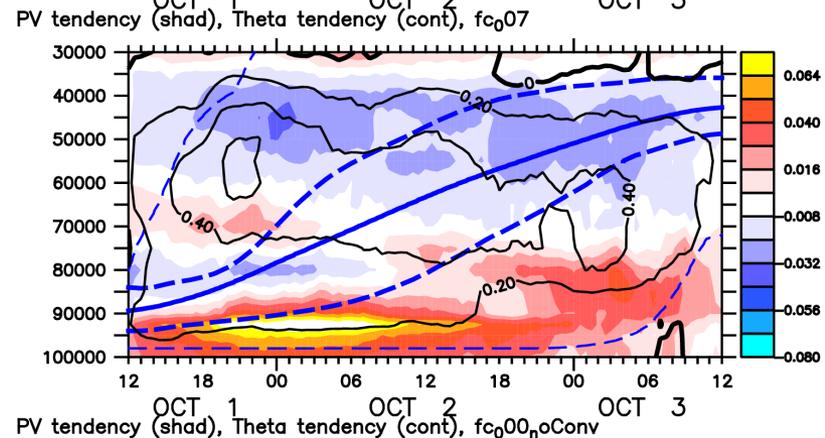
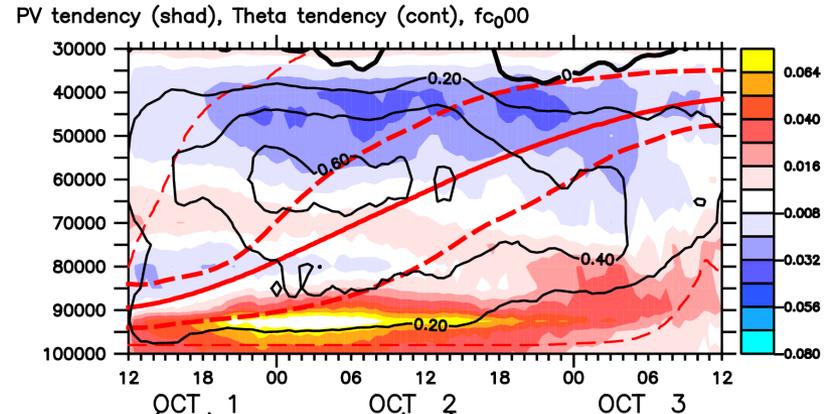
PV tendencies along trajectories



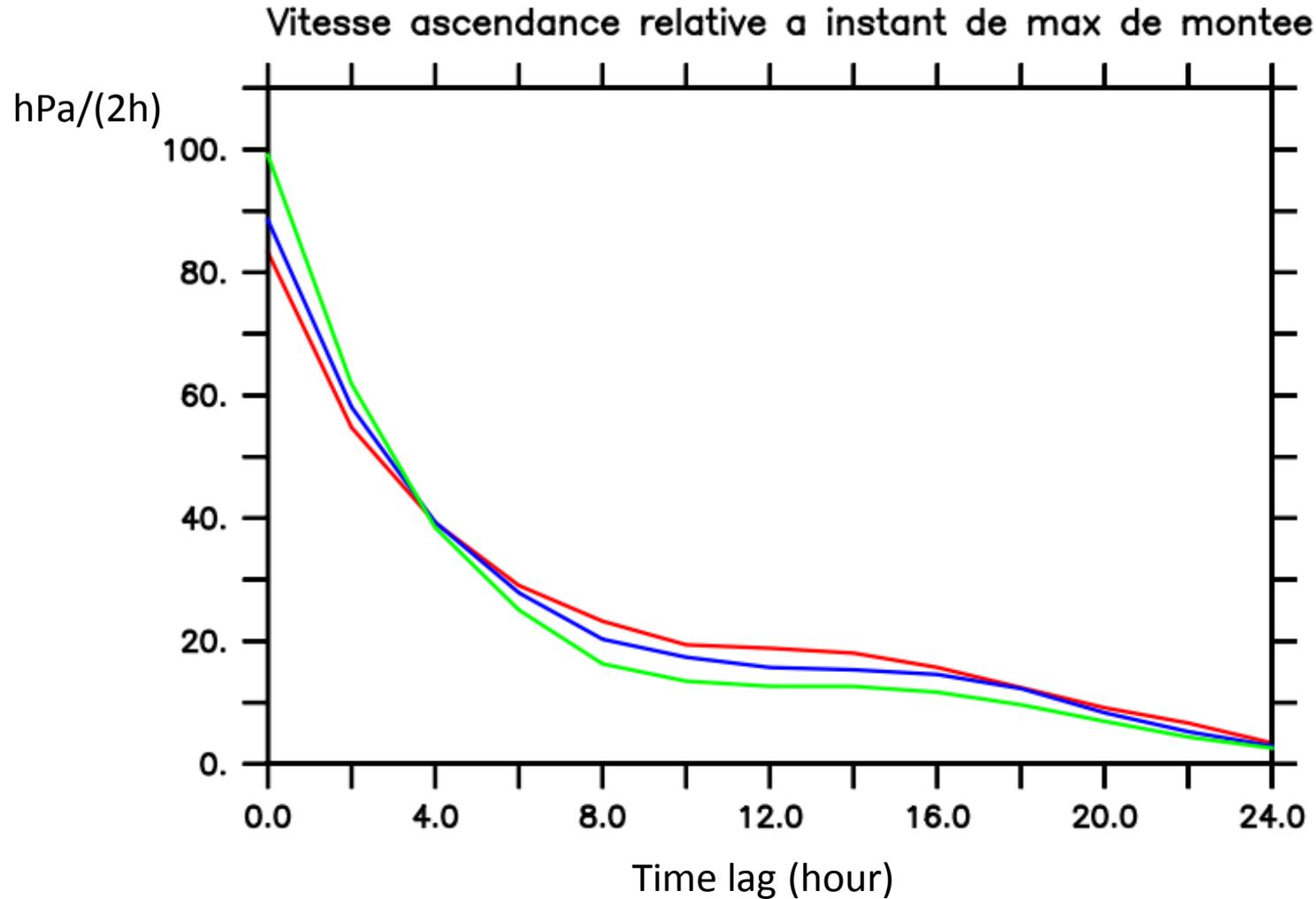
B85

PCMT

NoConv



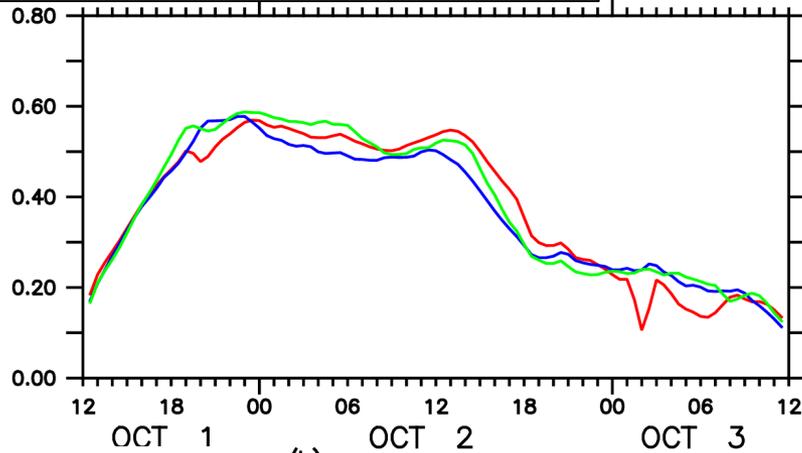
Ascending velocities



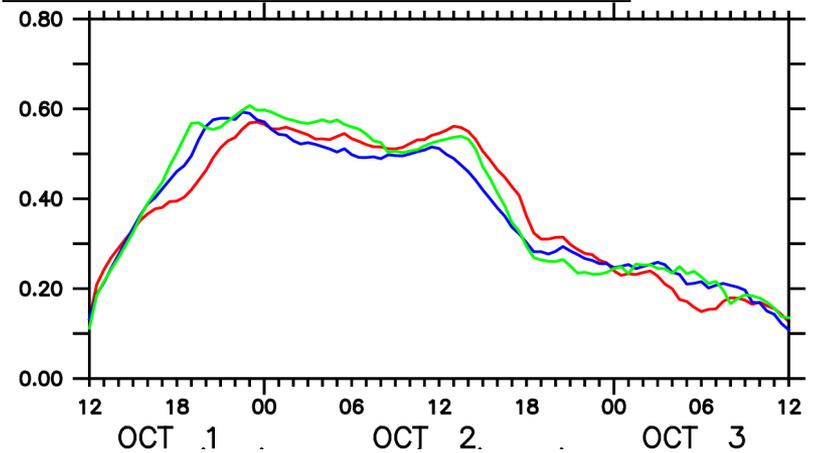
More rapid ascents in **NoConv** than **B85** at the time of maximum ascents but more sustained ascents in B85. **PCMT** is in between.

Heating and PV tendencies along trajectories

Rate of change of θ along traj K/h



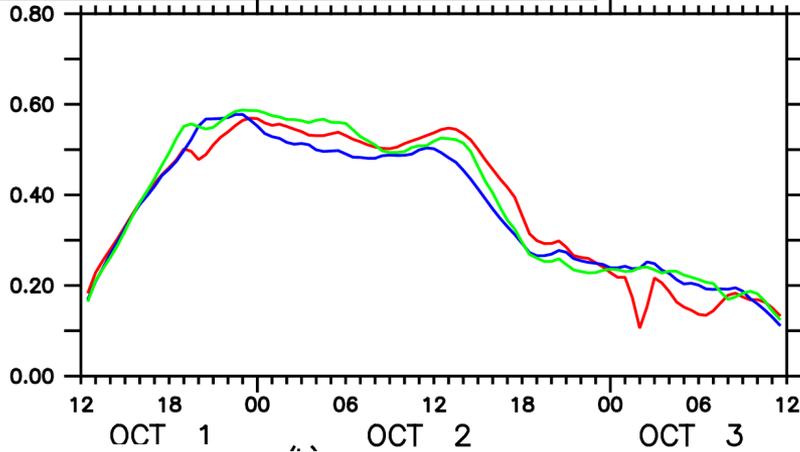
$$\dot{\theta} = \frac{\theta(t + 30 \text{ min}) - \theta(t - 30 \text{ min})}{\Delta t} + \mathbf{u} \cdot \nabla \theta(t) \quad \text{K/h}$$



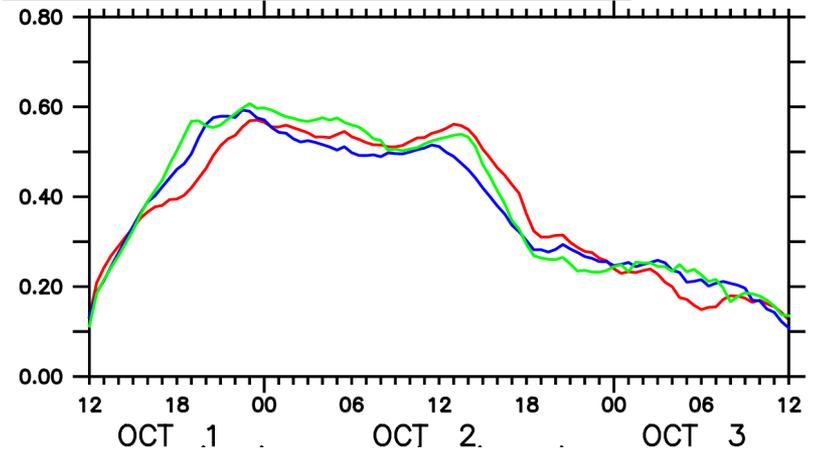
Consistency between heating rate fields computed with finite differences and variations in potential temperature along trajectories

Heating and PV tendencies along trajectories

Rate of change of θ along traj K/h

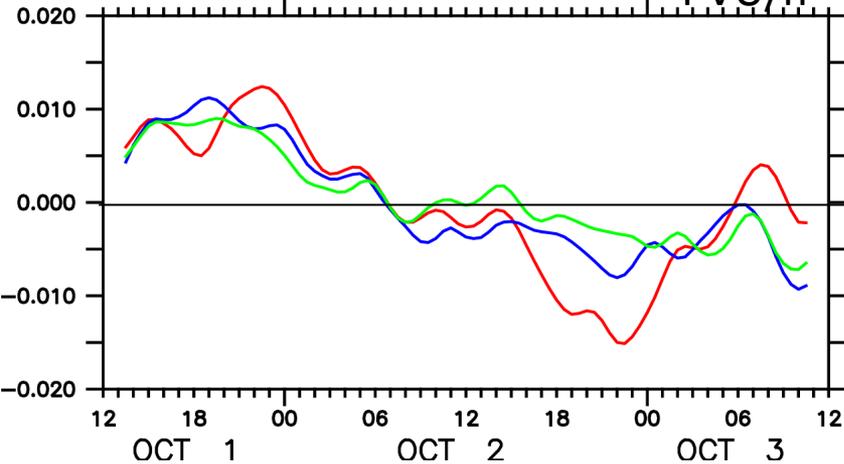


$$\dot{\theta} = \frac{\theta(t + 30 \text{ min}) - \theta(t - 30 \text{ min})}{\Delta t} + \mathbf{u} \cdot \nabla \theta(t) \quad \text{K/h}$$

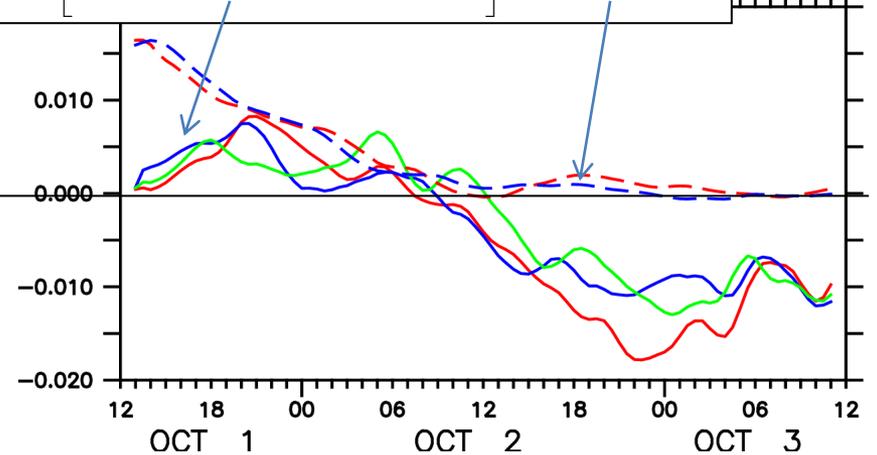


Rate of change of PV along traj

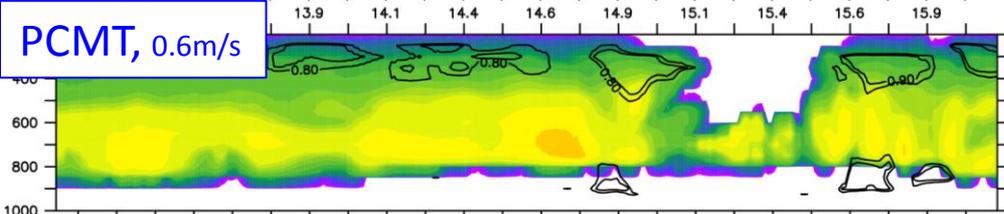
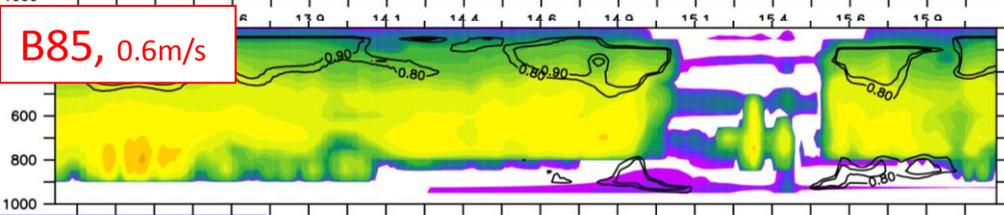
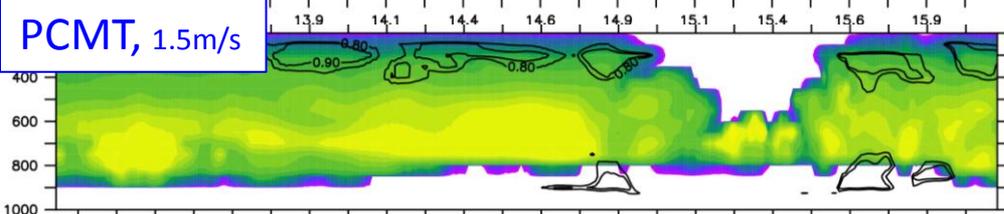
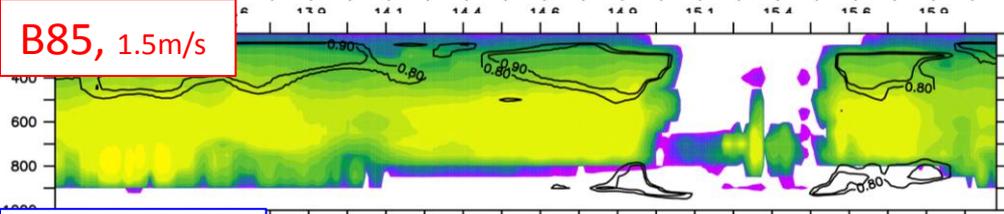
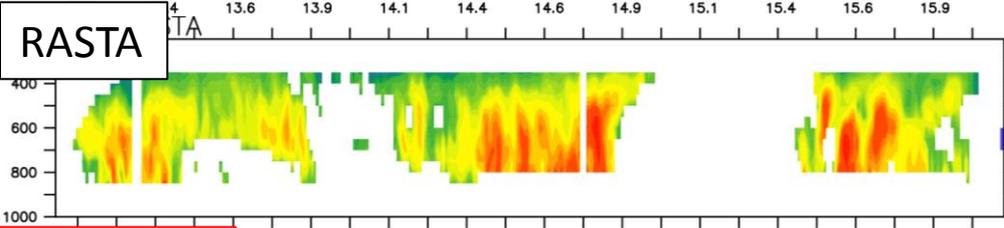
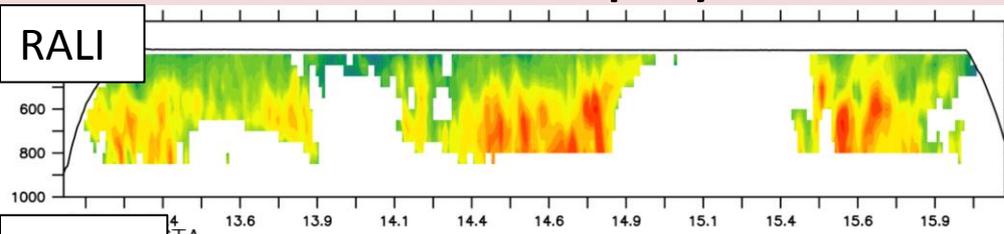
PVU/h



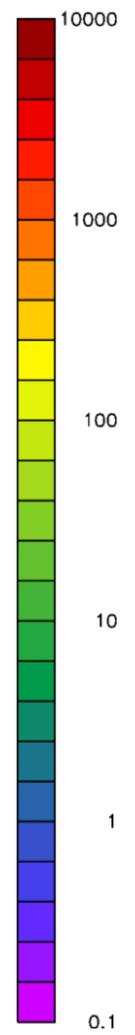
$$\frac{DPV}{Dt} = -g \left[(\zeta + f) \frac{\partial \dot{\theta}}{\partial p} + \frac{\partial u}{\partial p} \frac{\partial \dot{\theta}}{\partial y} - \frac{\partial v}{\partial p} \frac{\partial \dot{\theta}}{\partial x} \right] - g(\nabla \wedge \mathbf{F}) \cdot \nabla \theta \quad \text{PVU/h}$$



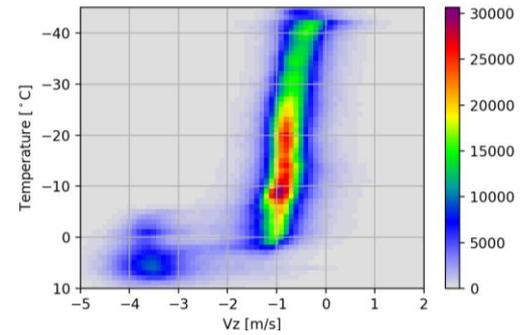
Microphysics: Ice water content F7



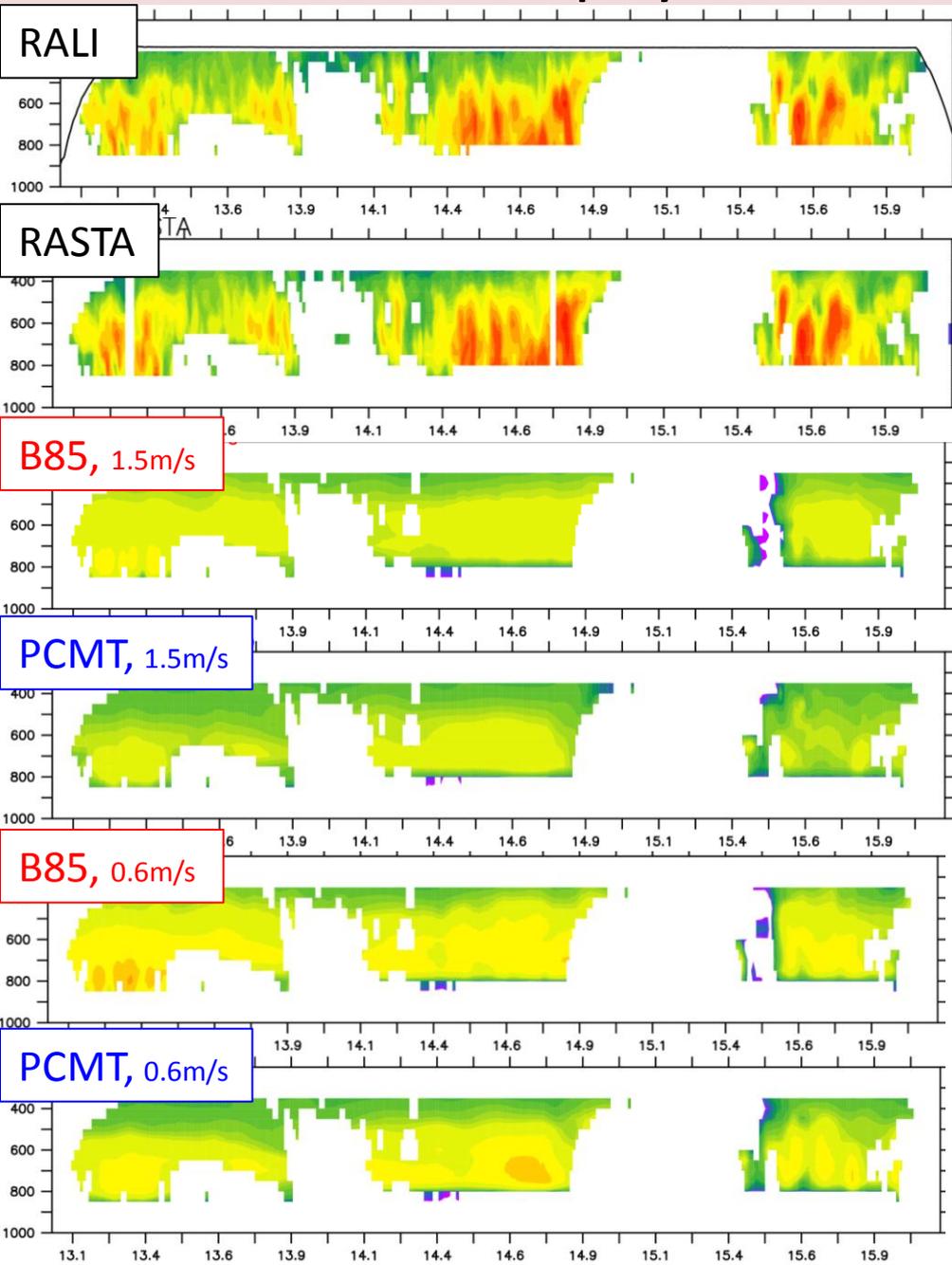
mg/m³



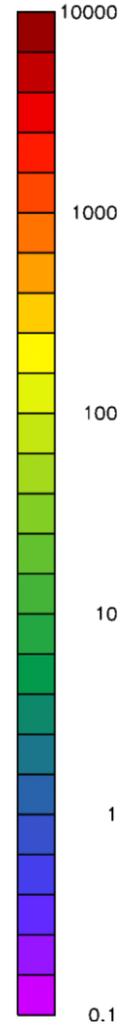
RASTA statistics of fall speed (V_{t+w})



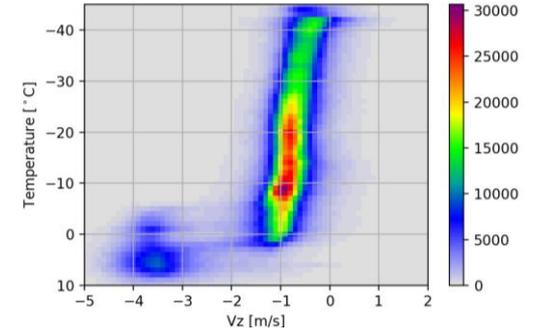
Microphysics: Ice water content F7



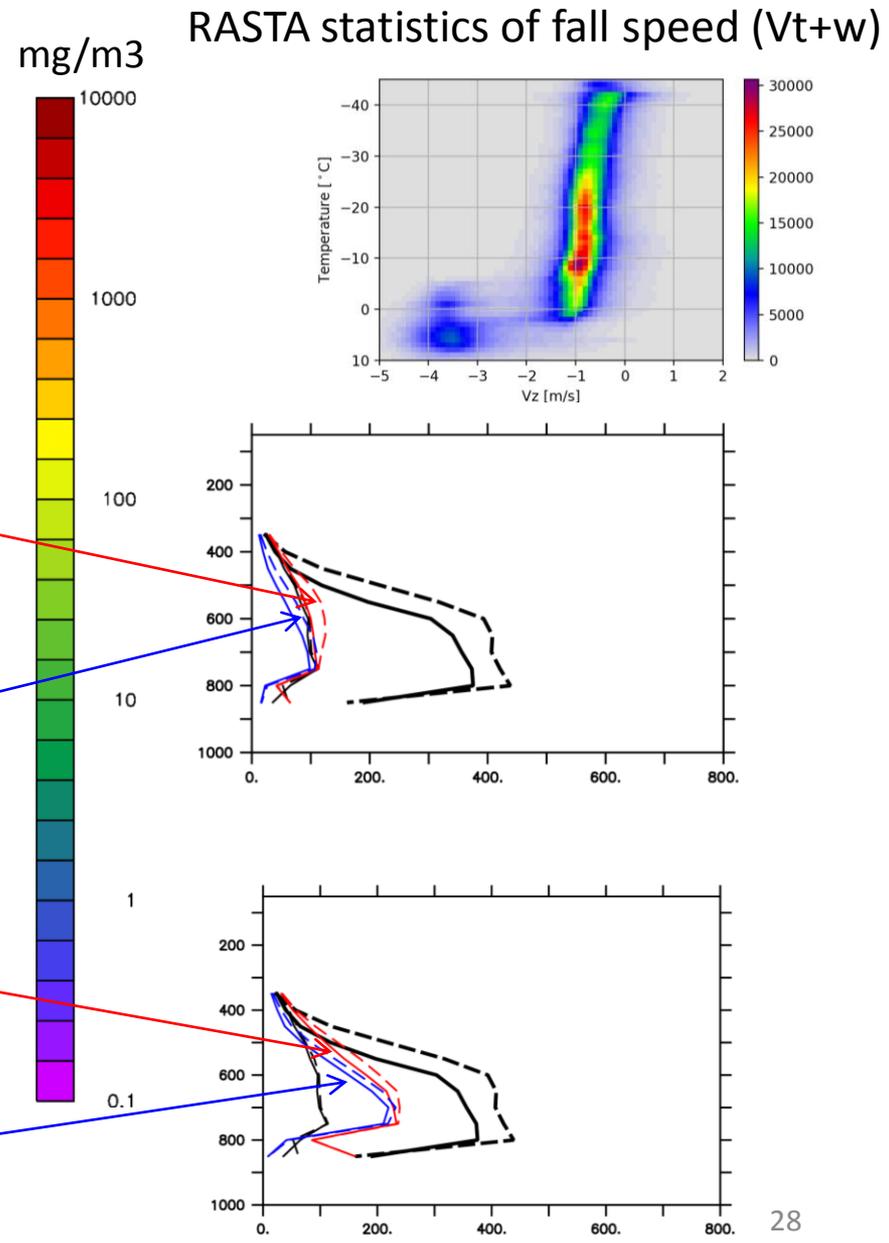
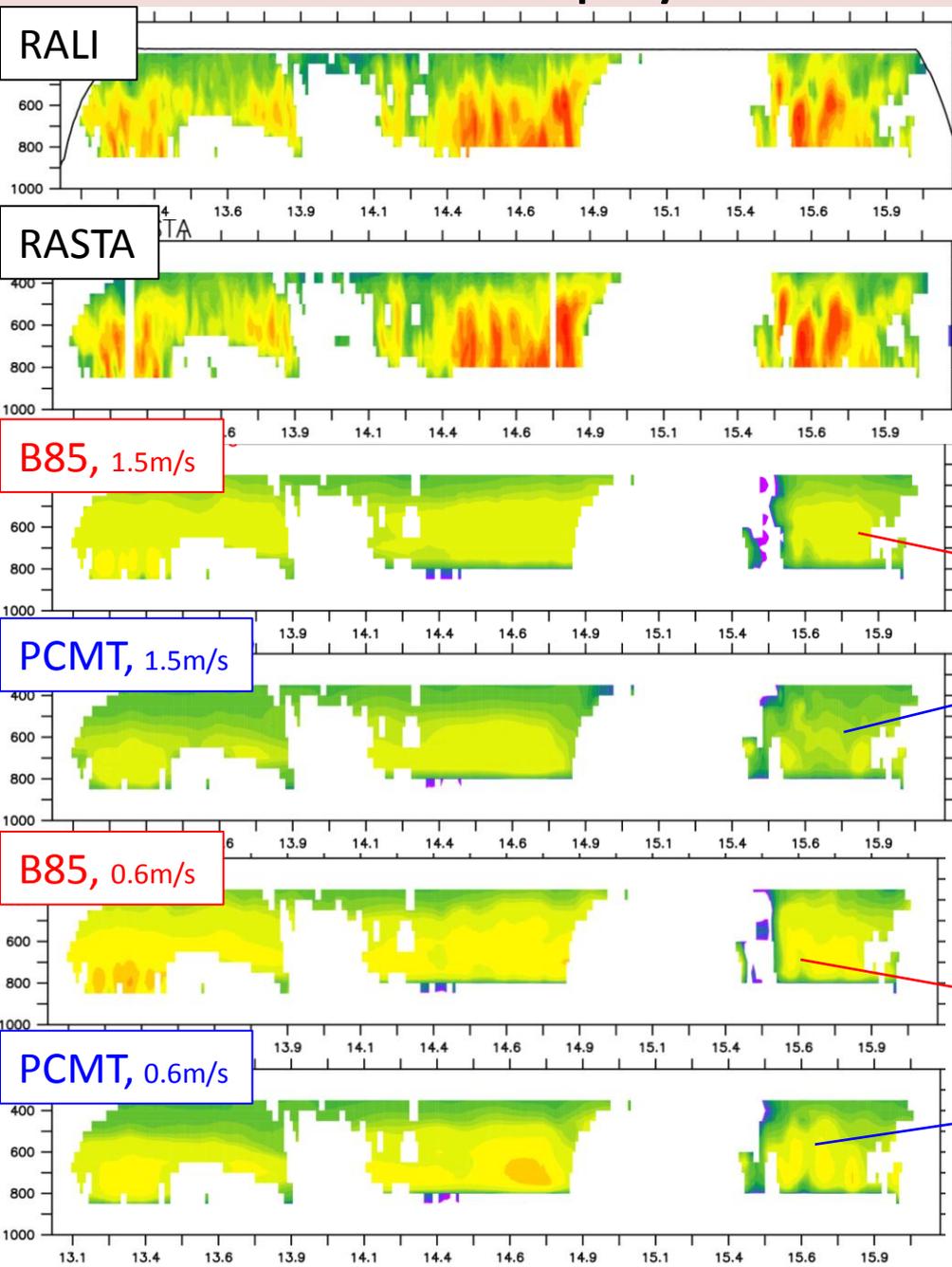
mg/m³



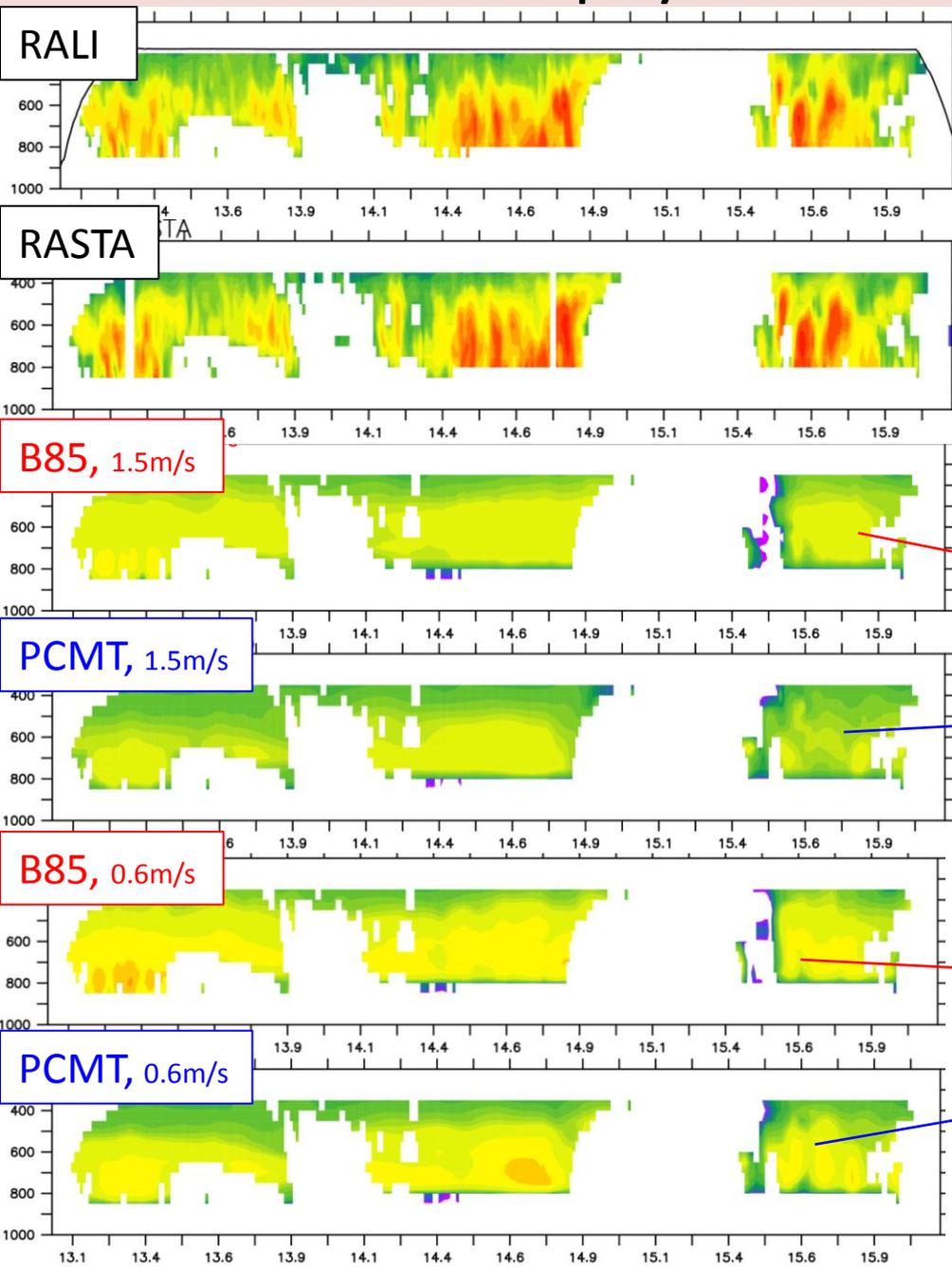
RASTA statistics of fall speed (V_{t+w})



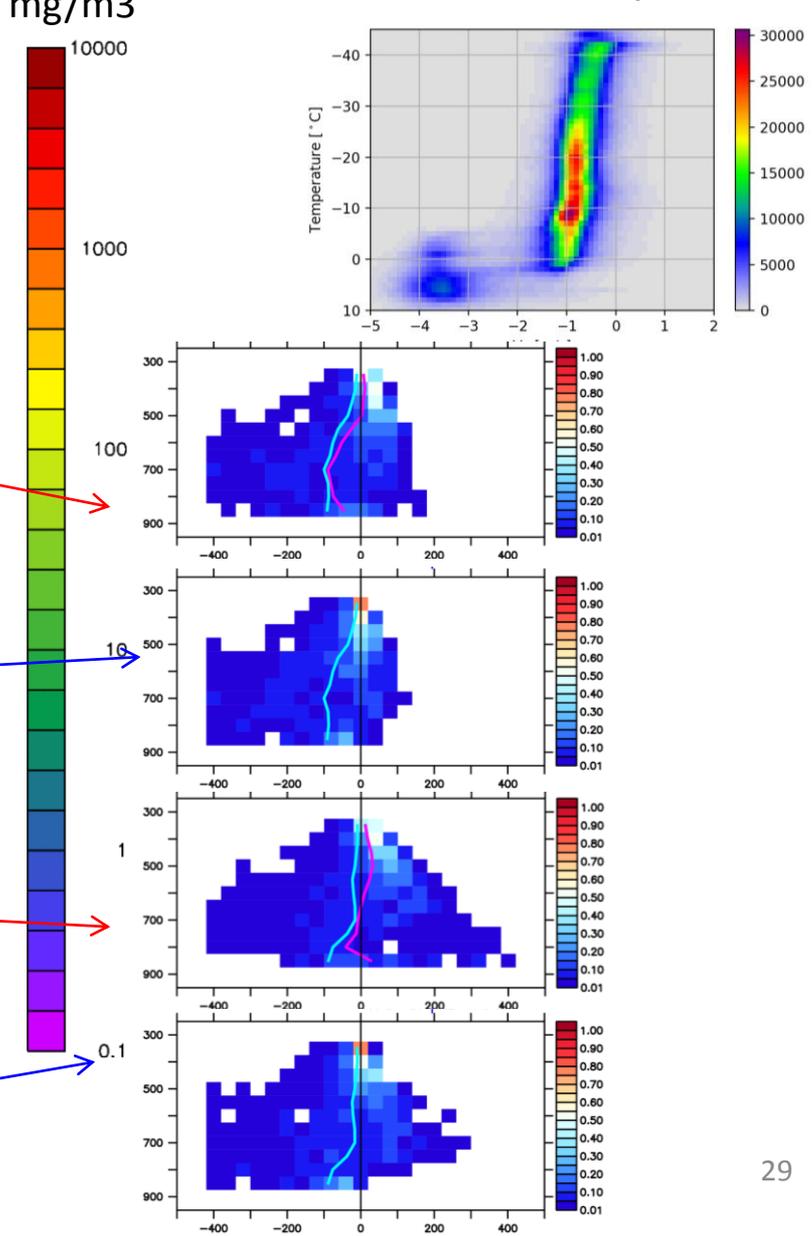
Microphysics: Ice water content F7



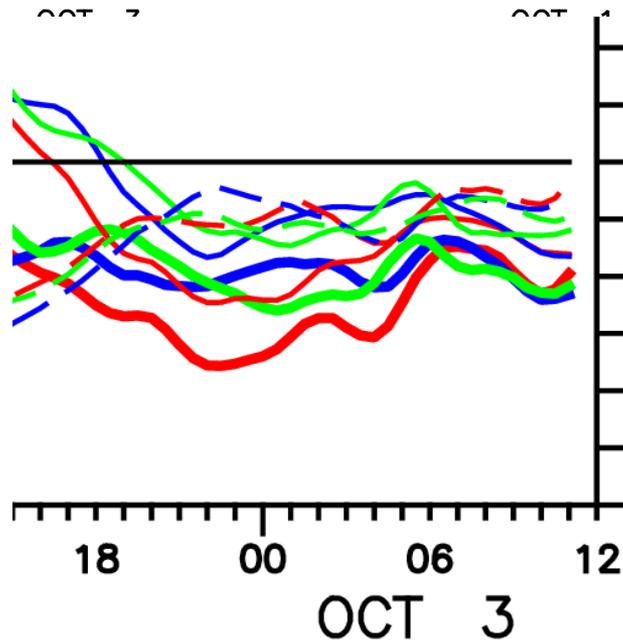
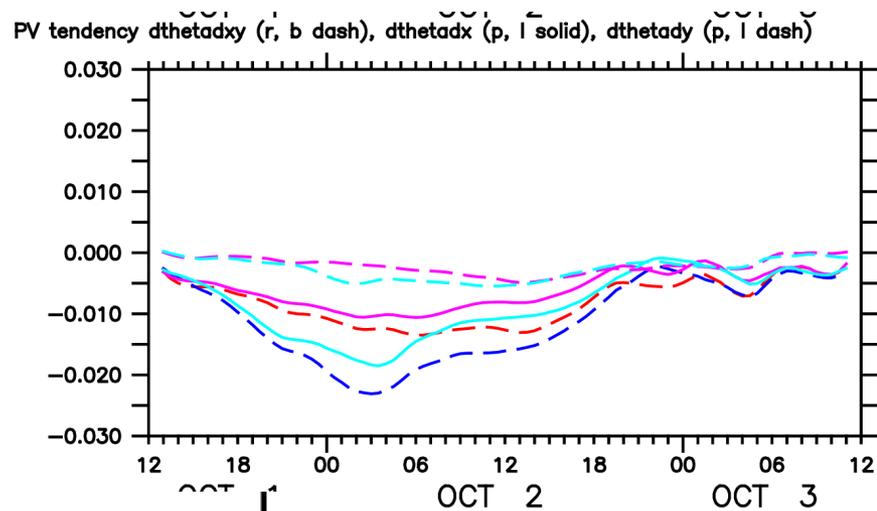
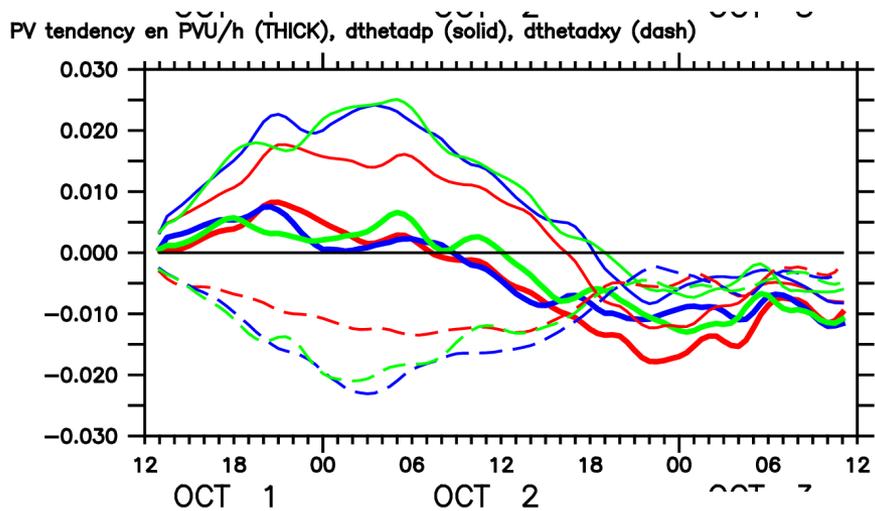
Microphysics: Ice water content F7



RASTA statistics of fall speed (V_{t+w})

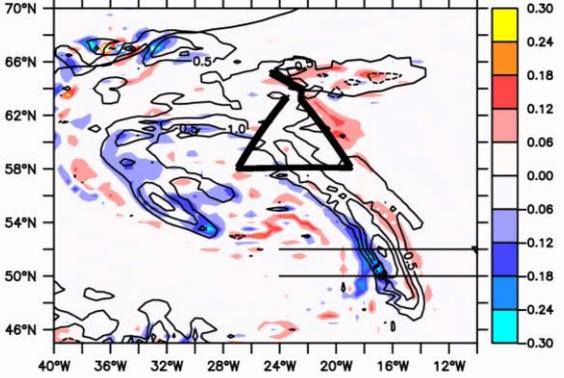


Heating and PV tendencies budgets

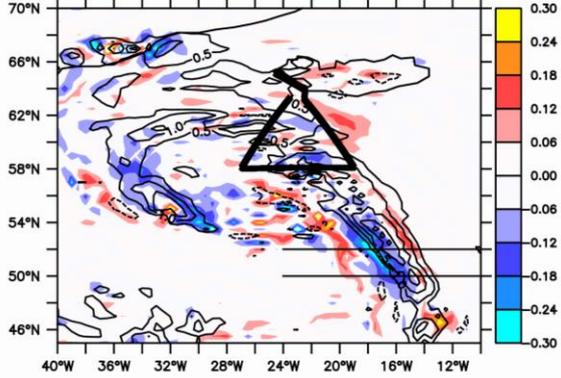


Heating and PV tendencies budgets (t0+24h)

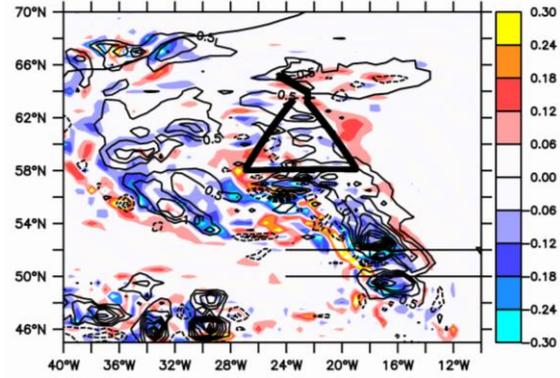
DPVDt, DthetaDt run0



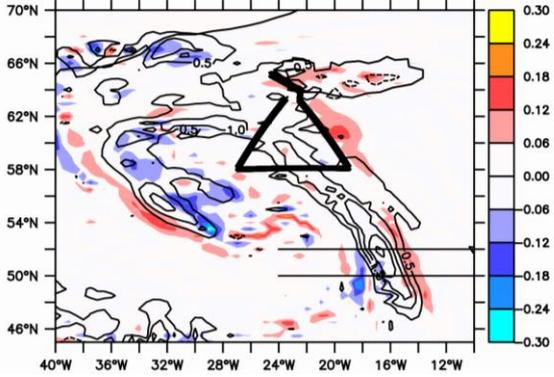
DPVDt, DthetaDt run7



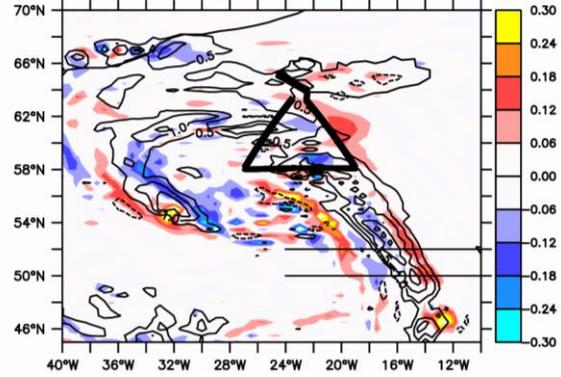
DPVDt, DthetaDt run0



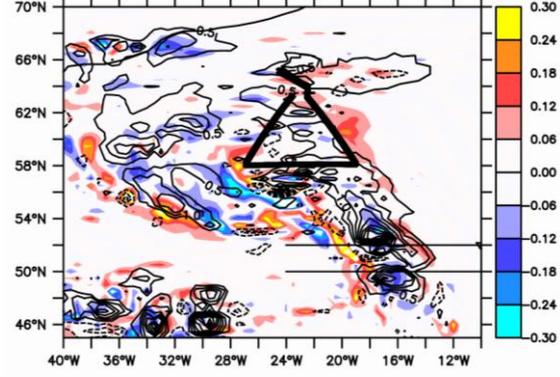
DPVDtp, DthetaDt run0



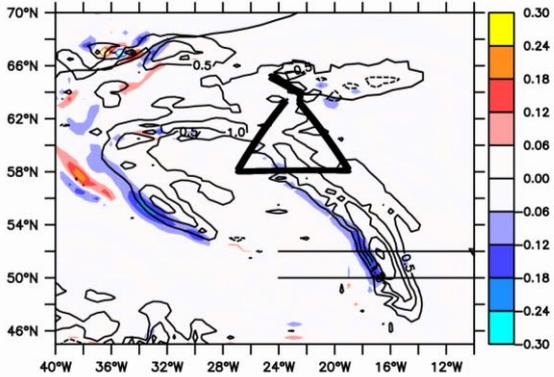
DPVDtp, DthetaDt run7



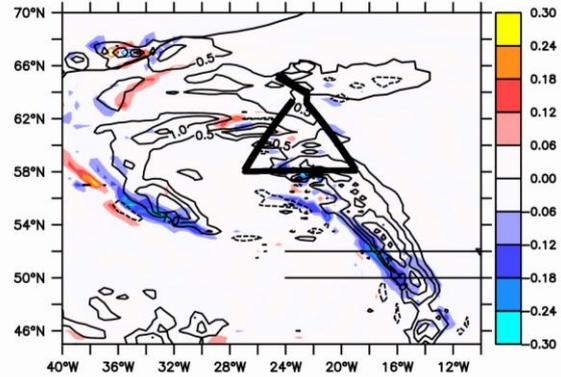
DPVDtp, DthetaDt run0



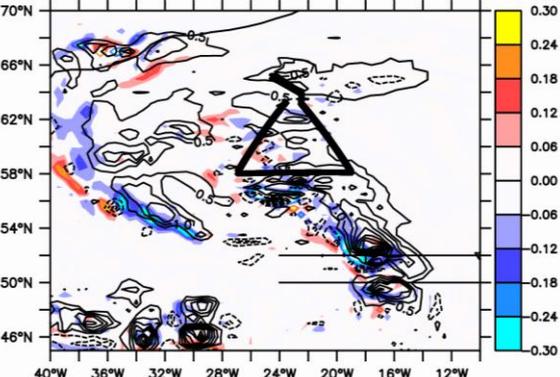
DPVDtxy, DthetaDt run0



DPVDtxy, DthetaDt run7



DPVDtxy, DthetaDt run0



Heating and PV tendencies budgets (t0+24h), 50N-52N

B85

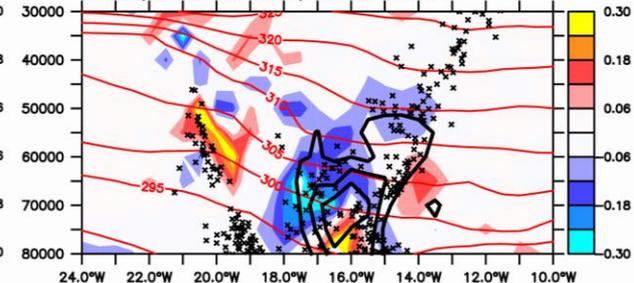
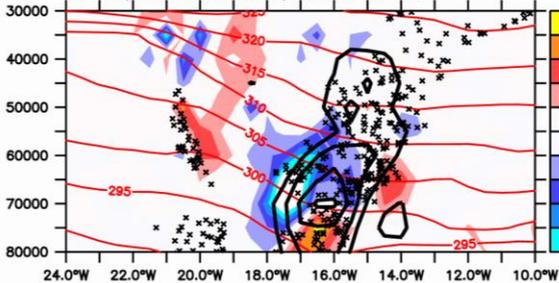
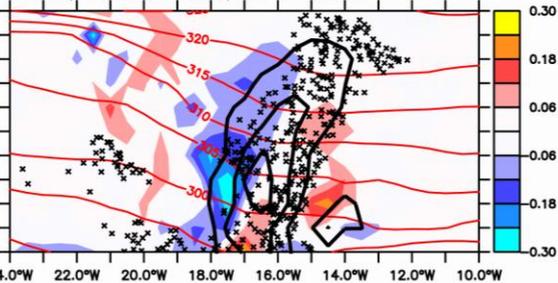
PCMT

NoConv

DPVDt, DthetaDt run0, 50:52 mean

DPVDt, DthetaDt run7, 50:52 mean

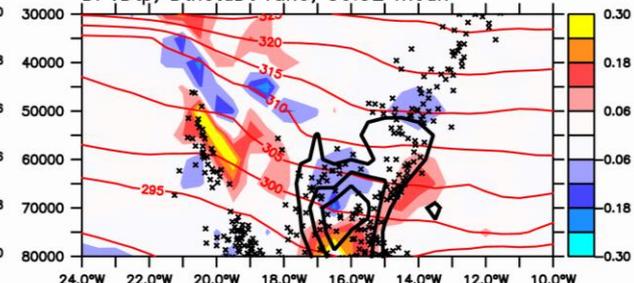
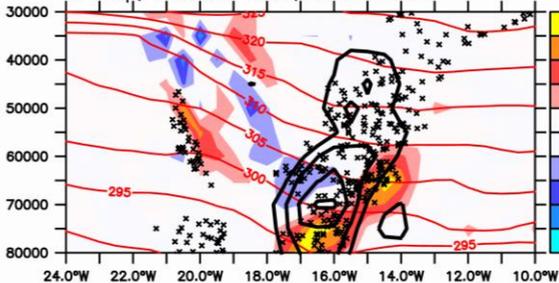
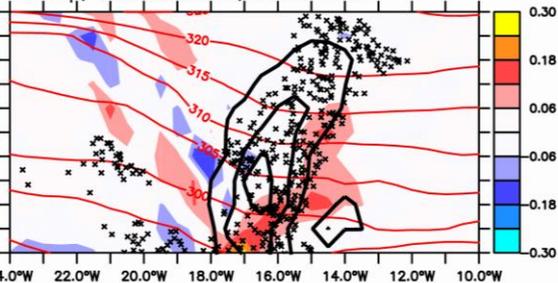
DPVDt, DthetaDt run0, 50:52 mean



DPVDtp, DthetaDt run0, 50:52 mean

DPVDtp, DthetaDt run7, 50:52 mean

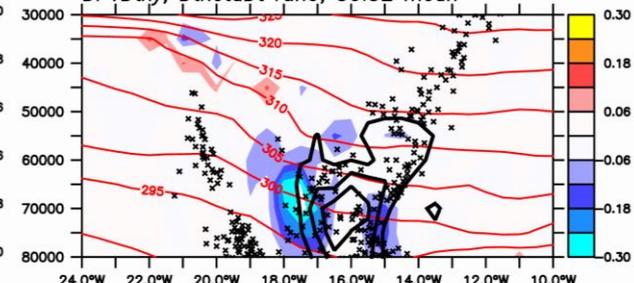
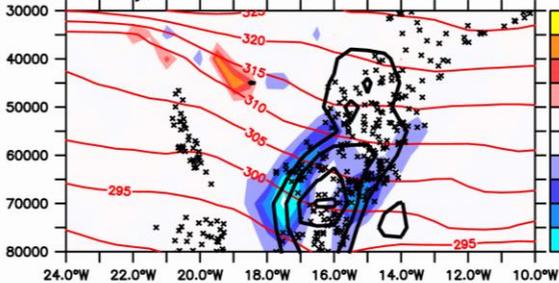
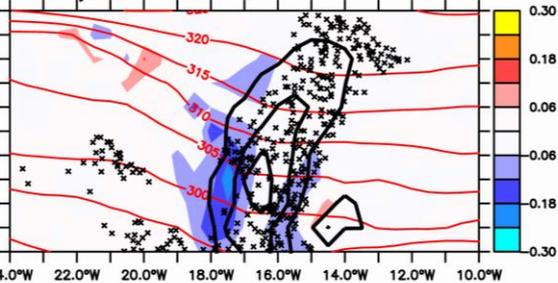
DPVDtp, DthetaDt run0, 50:52 mean



DPVDtxy, DthetaDt run0, 50:52 mean

DPVDtxy, DthetaDt run7, 50:52 mean

DPVDtxy, DthetaDt run0, 50:52 mean



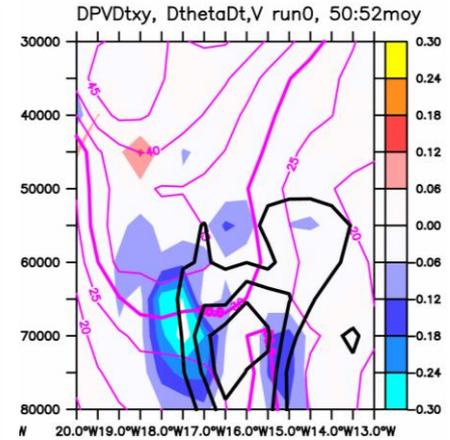
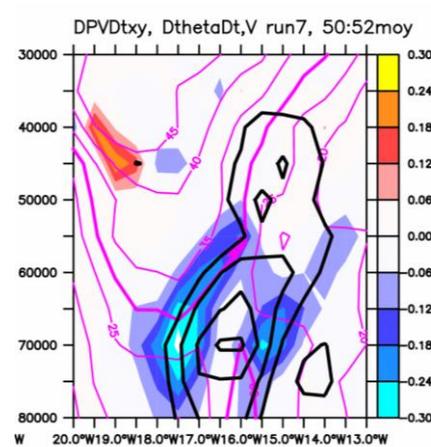
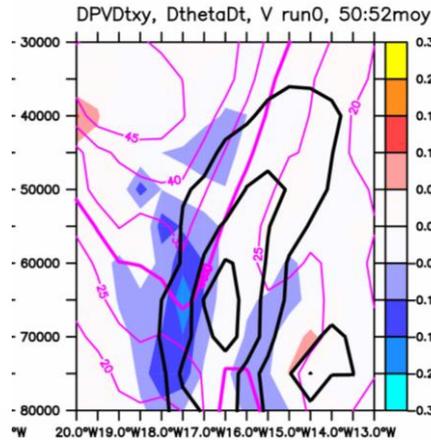
Understanding the negative PV tendency due to horizontal gradient of heating rate along the cold front

B85

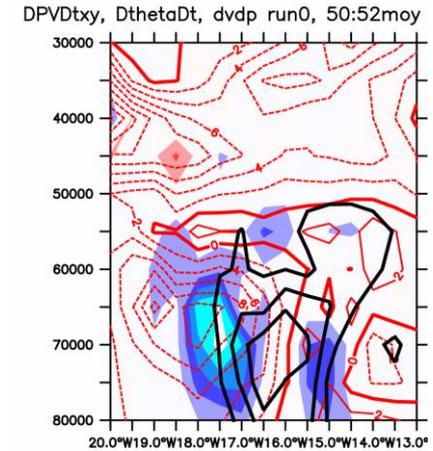
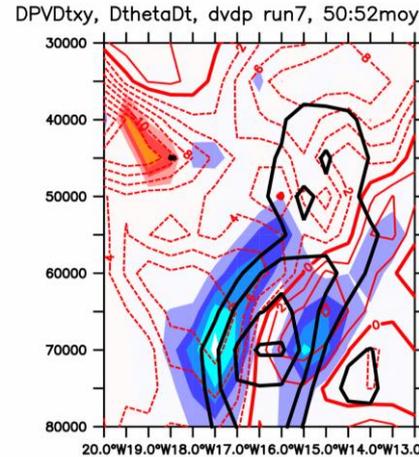
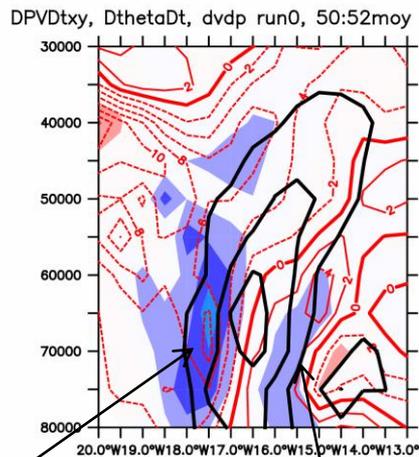
PCMT

NoConv

$$\frac{DPV}{Dt} = \dots + g \frac{\partial v}{\partial p} \frac{\partial \theta}{\partial x}$$



$$\frac{DPV}{Dt} = \dots + g \frac{\partial v}{\partial p} \frac{\partial \theta}{\partial x}$$

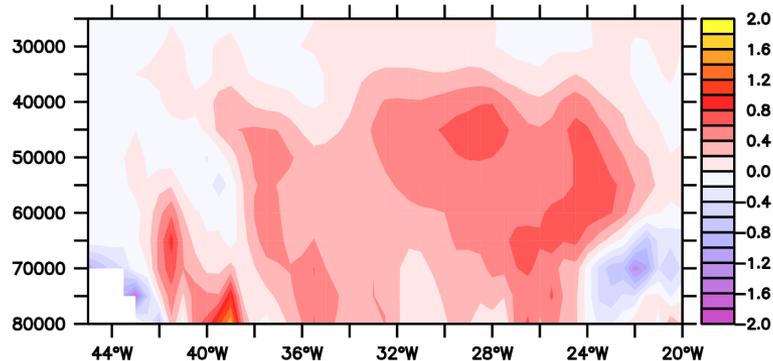


$$\frac{\partial v}{\partial p} < 0; \frac{\partial \theta}{\partial x} > 0$$

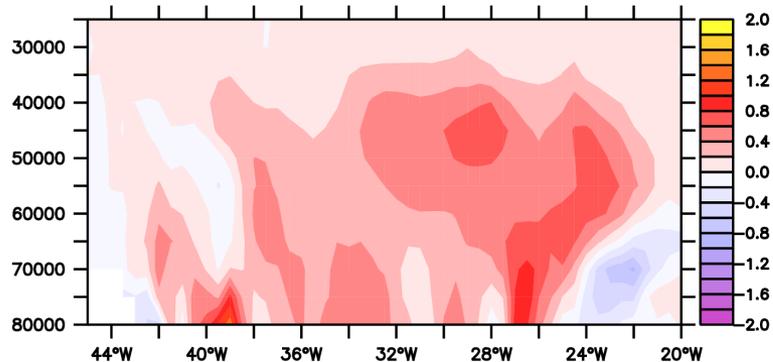
$$\frac{\partial v}{\partial p} > 0; \frac{\partial \theta}{\partial x} < 0$$

Eulerian Heating rate budget after 24h

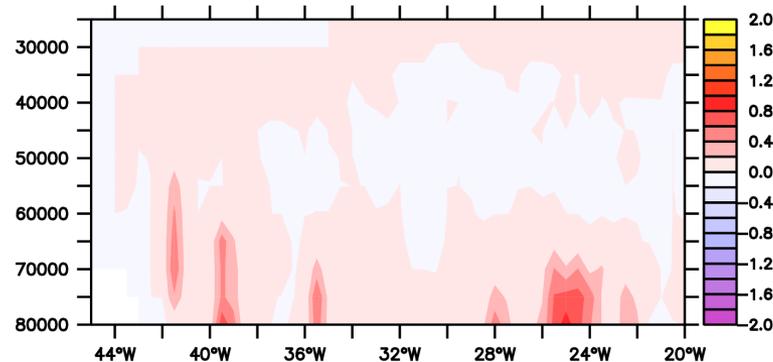
0 Total heating 63N–65N



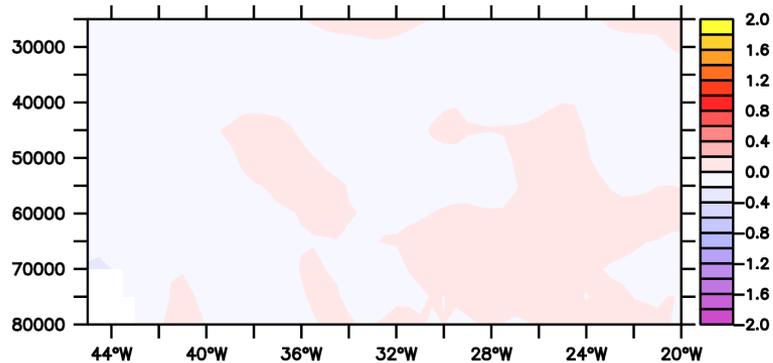
0 stratiforme 63N–65N



0 convectif 63N–65N



0 rayonnement 63N–65N



0 frottement 63N–65N

